

Richard Harris

**Buro Happold
&
University of Bath**

TIMBER- THE KEY TO TOMORROW`S ENVIRONMENT

Arches and Shells in Timber

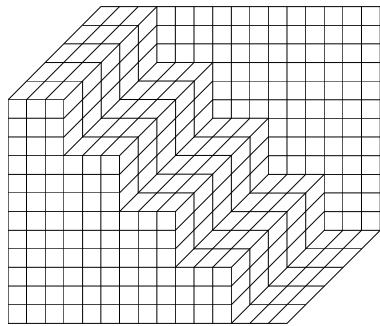
Tallinn

November 27th 2008

Richard Harris

Buro Happold

Technical Director



Buro Happold



Richard Harris

University of Bath

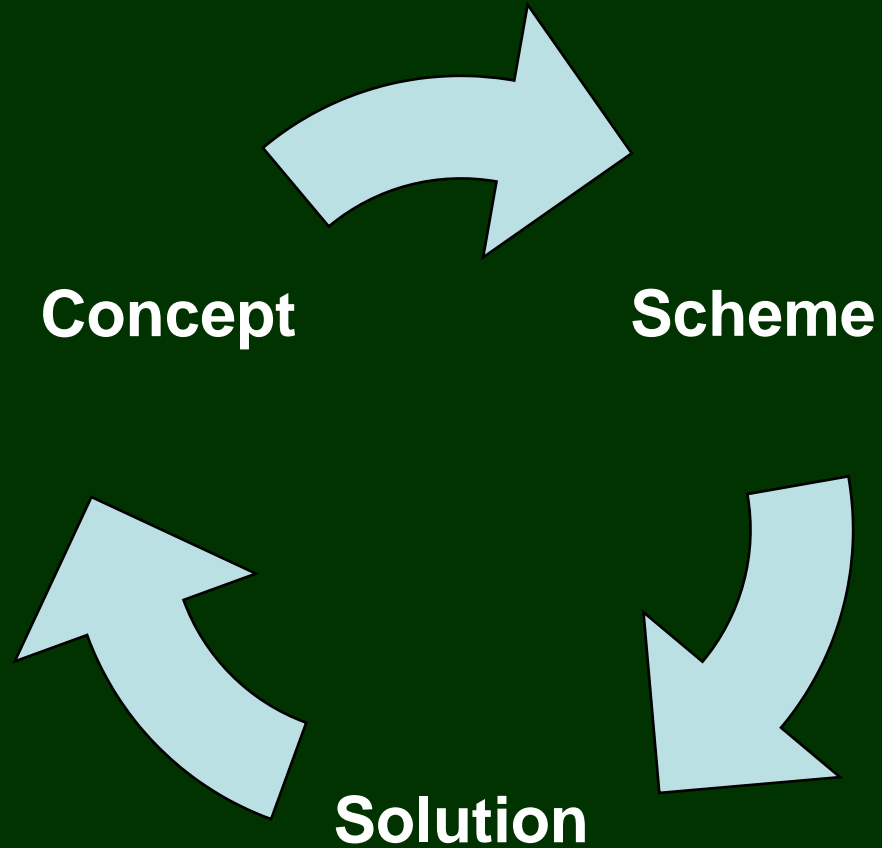
**Professor of
Timber Engineering**



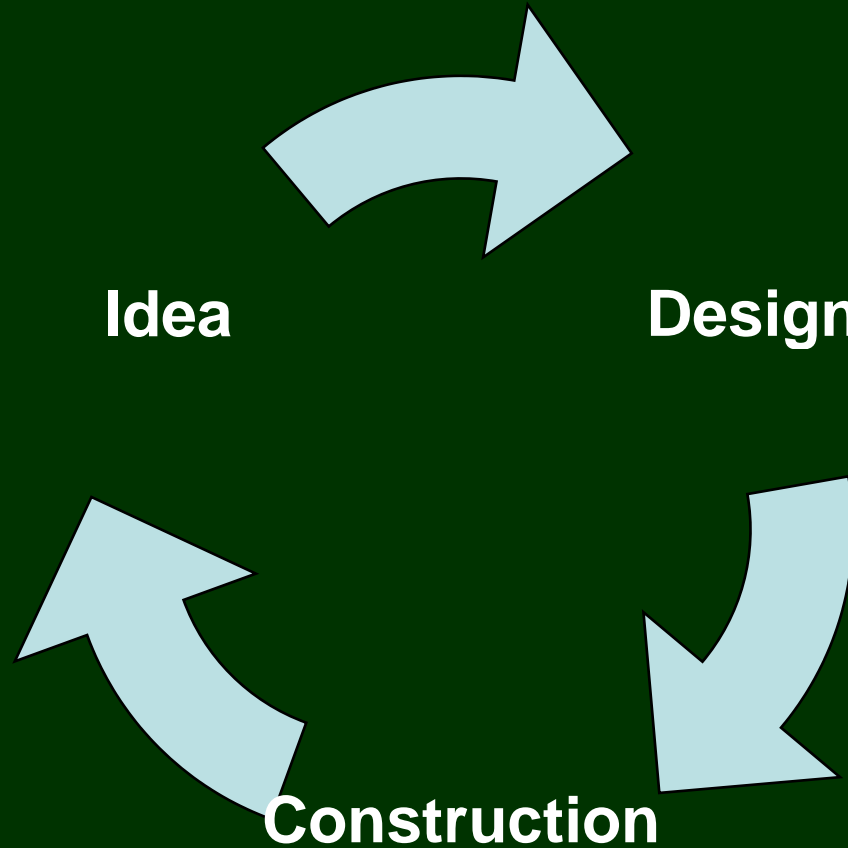
Richard Harris
Timber Engineer



The Design and Construction Process



The Design and Construction Process



The Use of Roundwood

a basic material

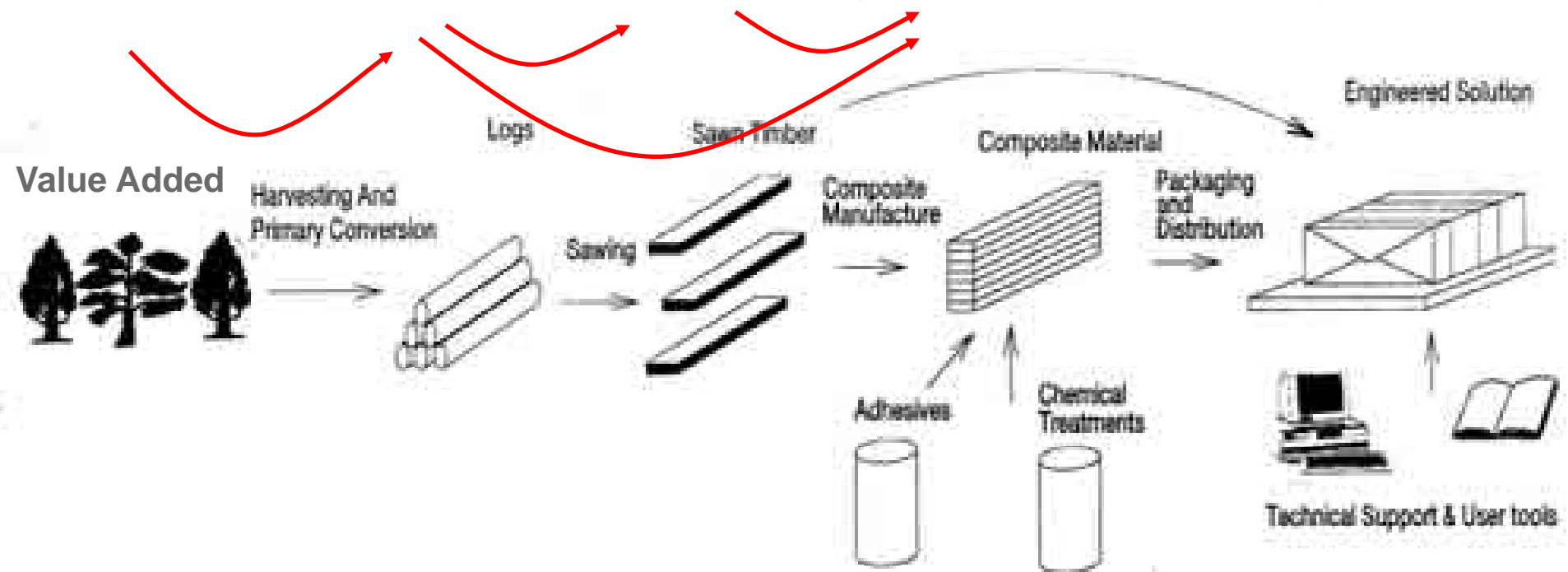
The Use of Roundwood

low grade timber

low environmental impact

Background - The Timber Production Process

low cost material



The Client Brief

1. For improved quality and early added value, at 20 years thin to one tree per 11 m².

- This releases value to be used in better management

2. At 30-35 years: - Clear fell

- Use trees not suitable for sawn timber



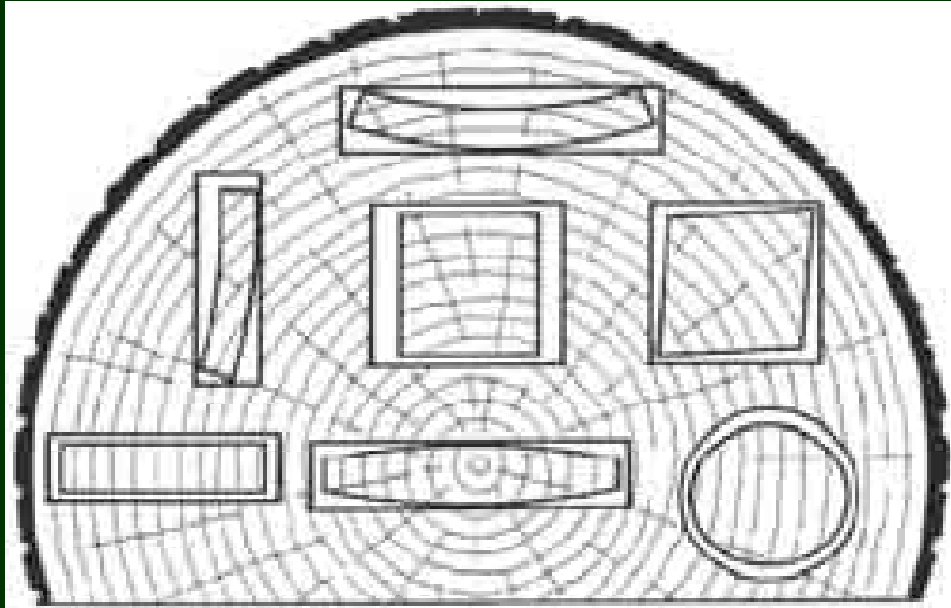
The Material – Norway Spruce

Thinned/poor quality trees:

- small diameter
- 180-220 mm at 1 metre
- 75-100mm at 10-15 metres



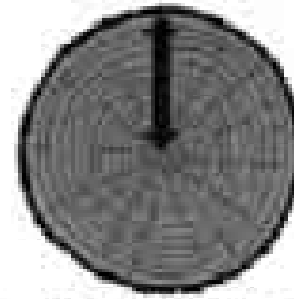
The Advantages of Roundwood



THE EFFECT OF SHRINKAGE



Tangential Shrinkage
 $\approx 2 \times$ Radial Shrinkage



Radial Shrinkage



Very Little Longitudinal
Shrinkage

General rules for roundwood properties

- **Mechanical properties:**
 - same strength wood as sawn timber
 - therefore same related standards can be applied to the round timber as sawn timber
- **Knot angle is optimum**
 - knot area minimised on surface.



General rules – now

- To design using roundwood
 - choose grading criteria
 - visual or strength related
 - FAIR CT 95-0091. VTT - 1999
 - carry out tests
 - grade the timber
 - using guidelines choose a grade and design with EC5

The solution– 1985 -1995

- **To design using roundwood**
 - **choose grading criteria**
visual or strength related
 - **carry out tests**
as deemed appropriate
 - **Grade the timber**
into appropriate BS5268 Pt 2 classes



Hooke Park College, Dorset, England

The idea

To design modern buildings with a poor quality material

To add value to a low value product

Hooke Park College, Dorset, England

The complication

Material with unknown properties

No recognised code or grading

Material with variable dimensions

Hooke Park College, Dorset, England

The solution:

Modern architecture

Fundamental understanding of material

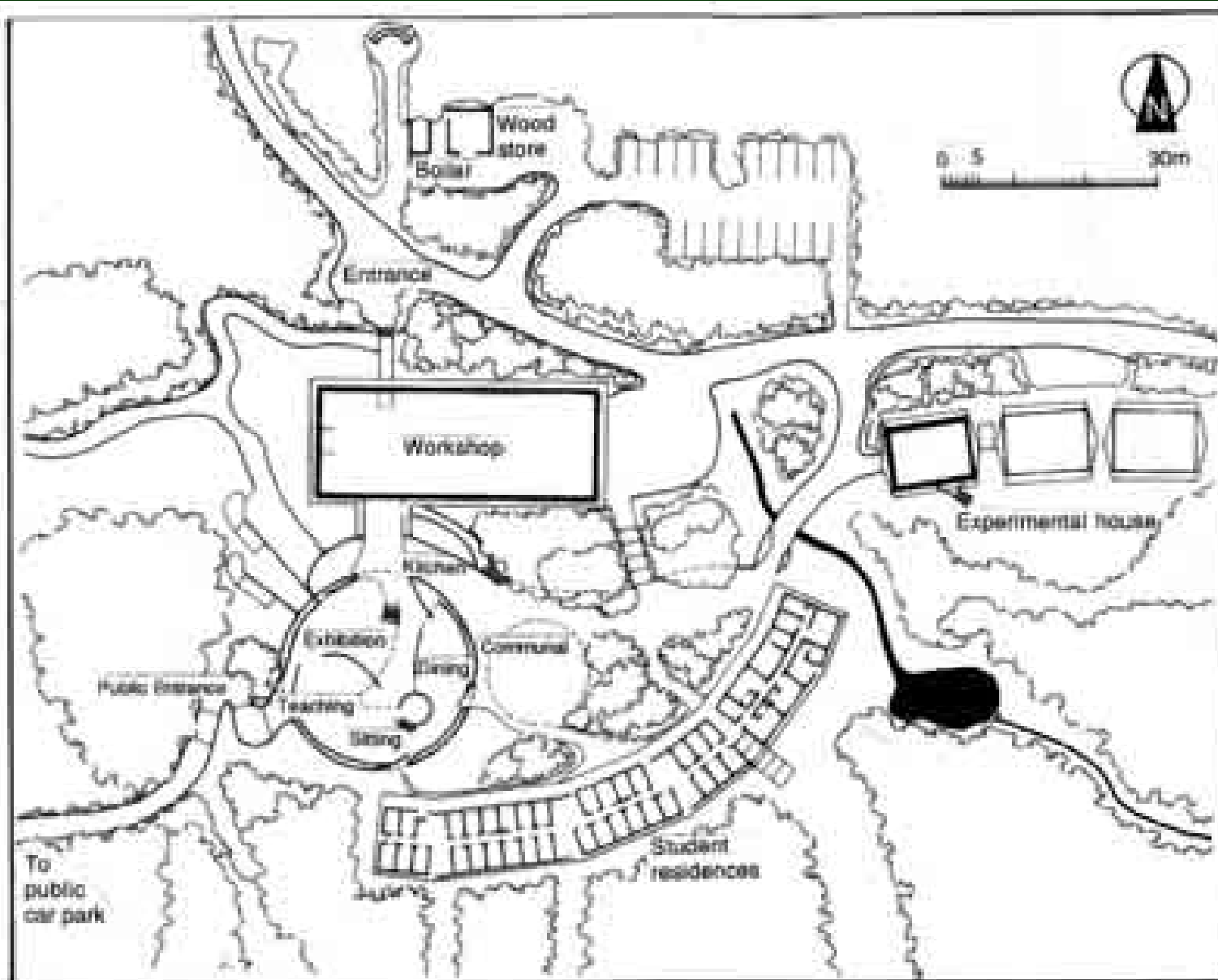
Innovative jointing

New construction techniques



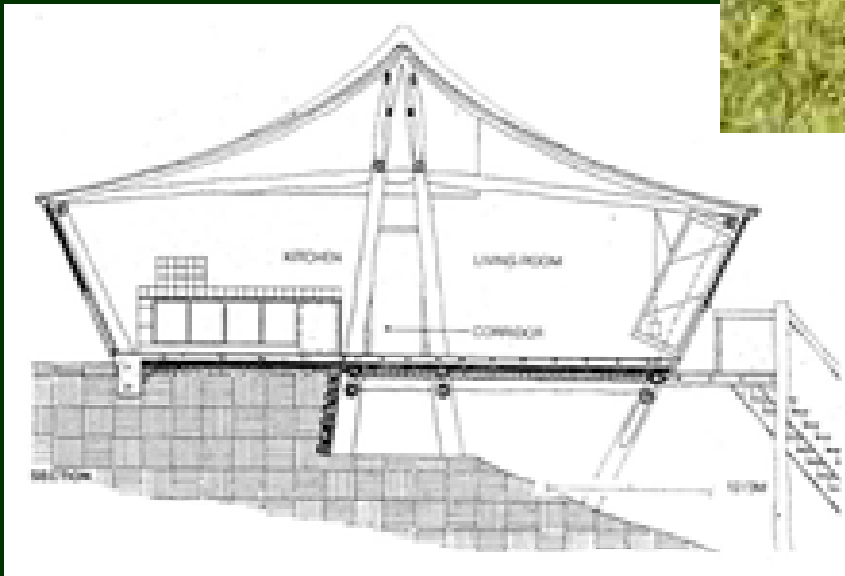




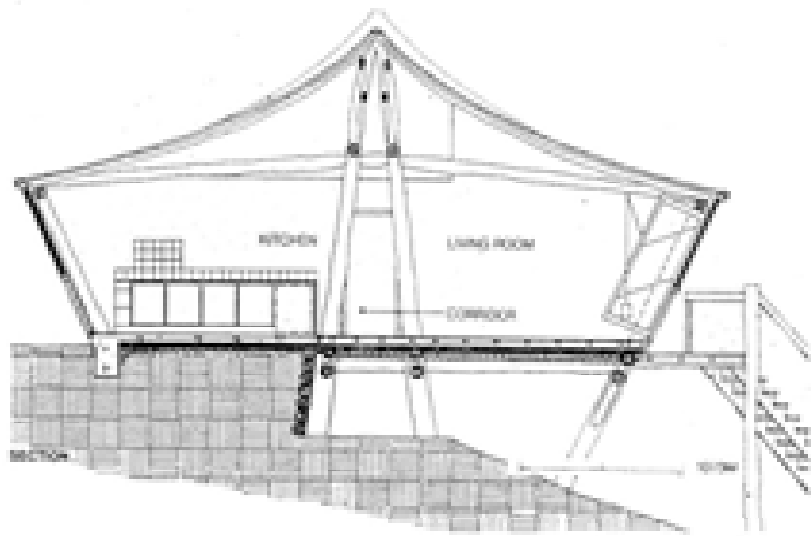


Hooke Park College, Dorset - Prototype House

1984



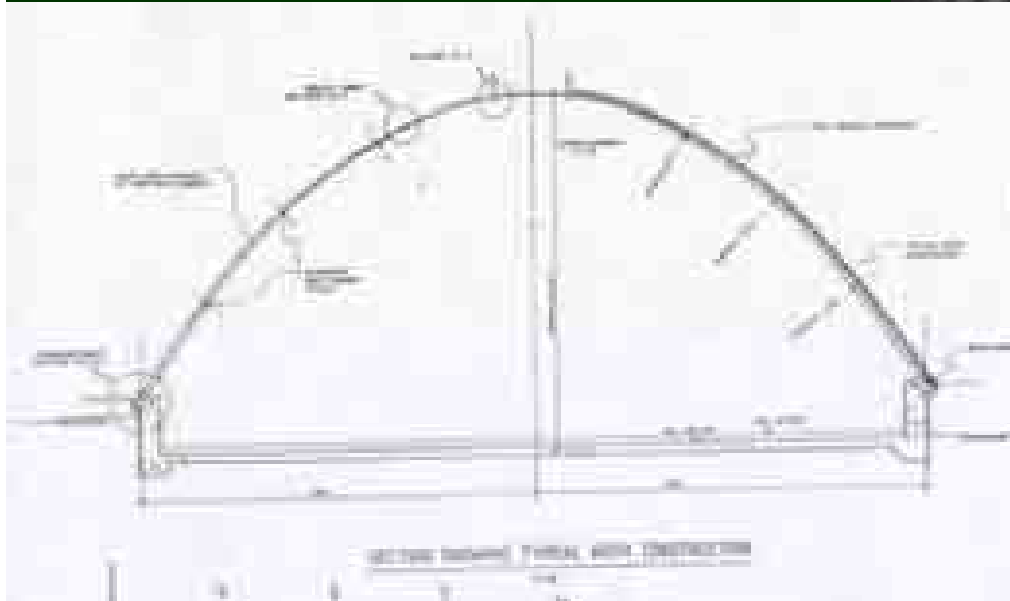


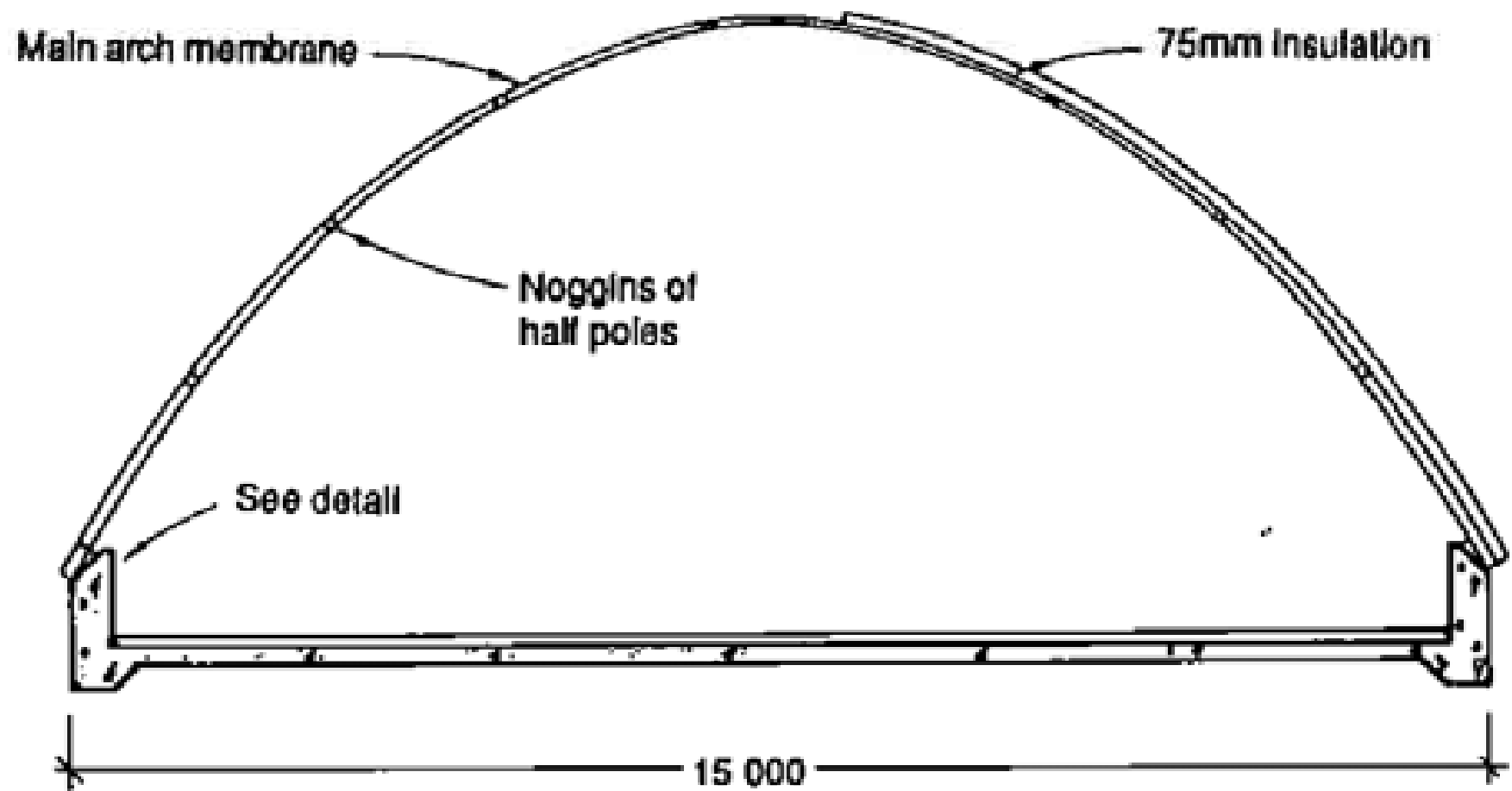




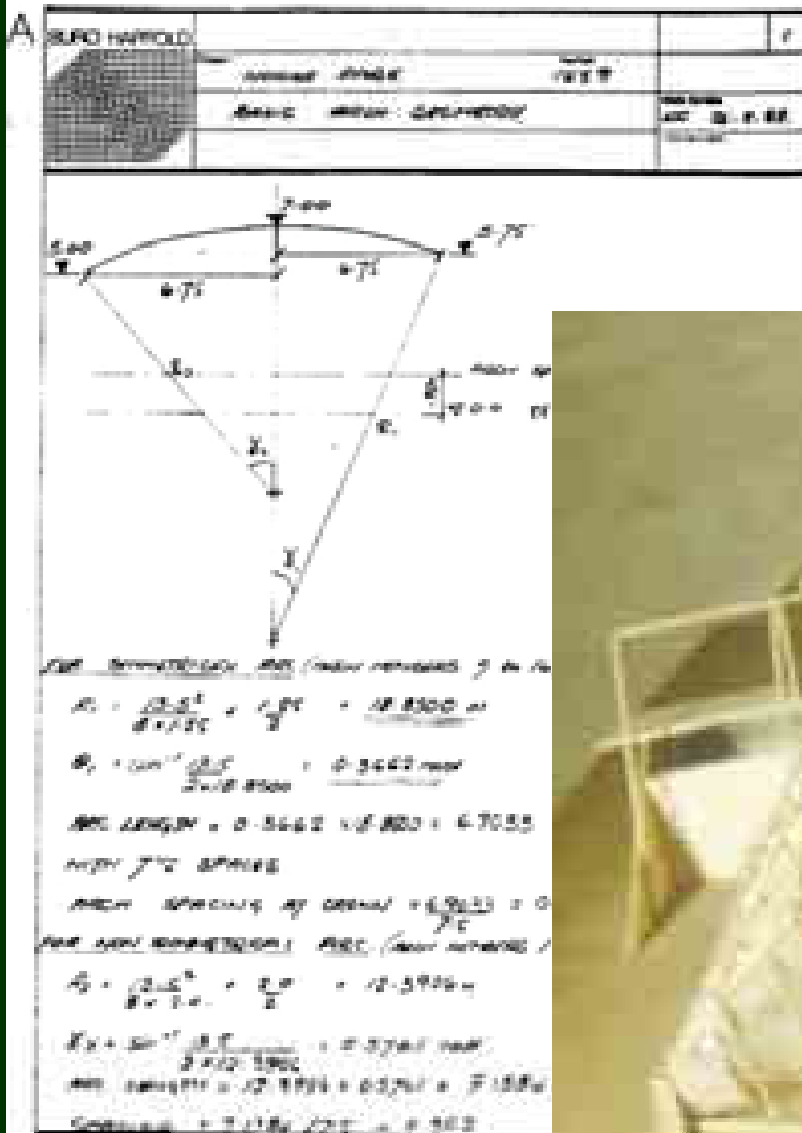
Hooke Park College, Dorset - Workshop

1991





Modelling structure



Working with the Material

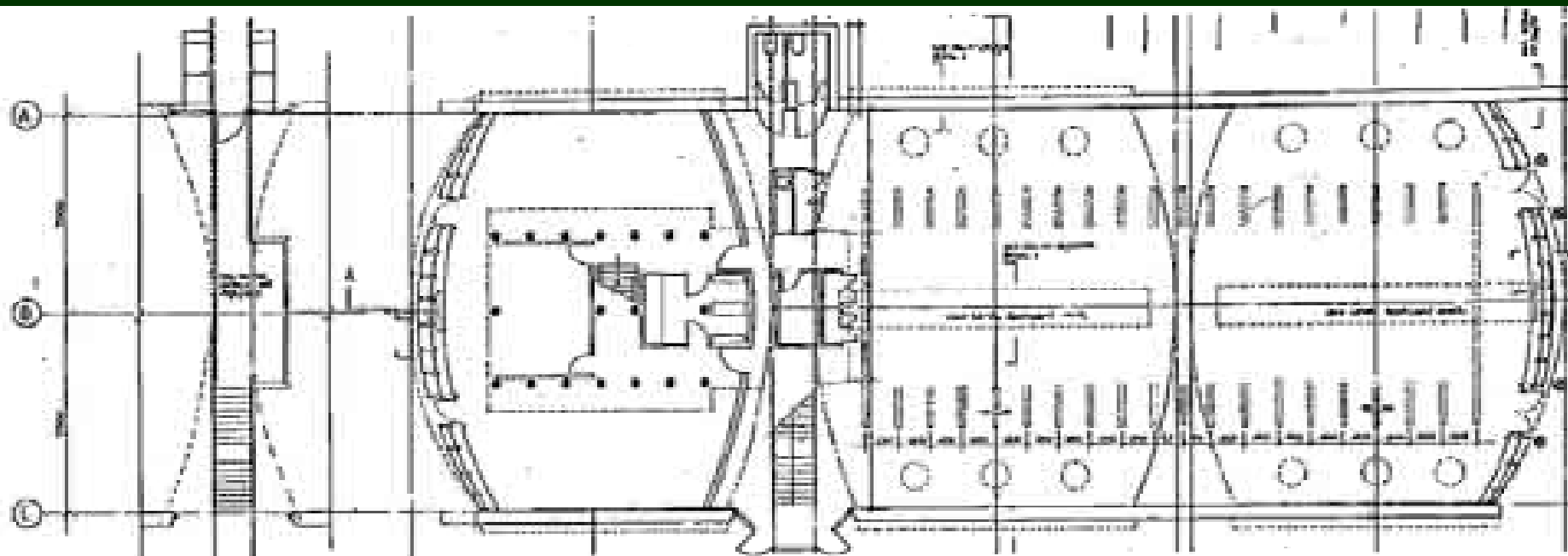


Full size prototyping

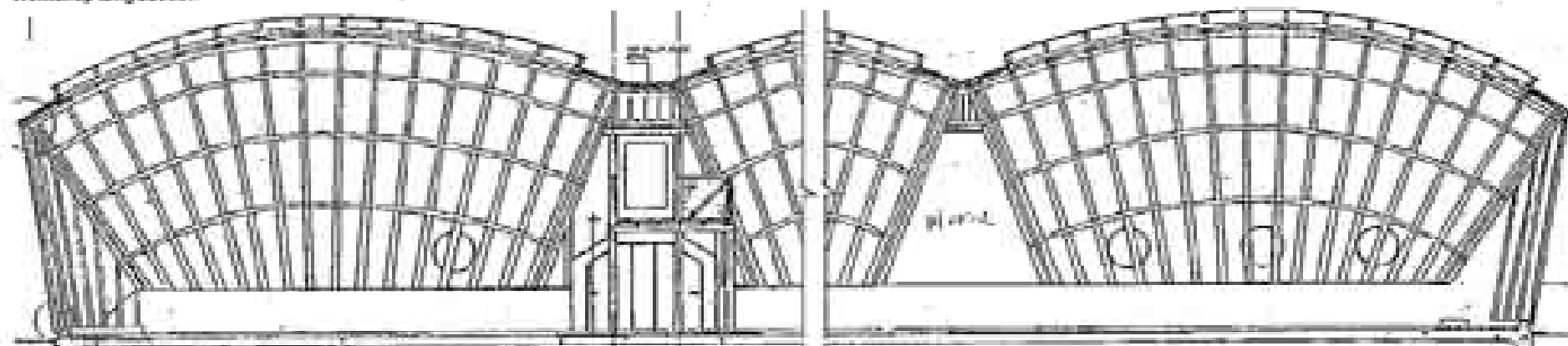


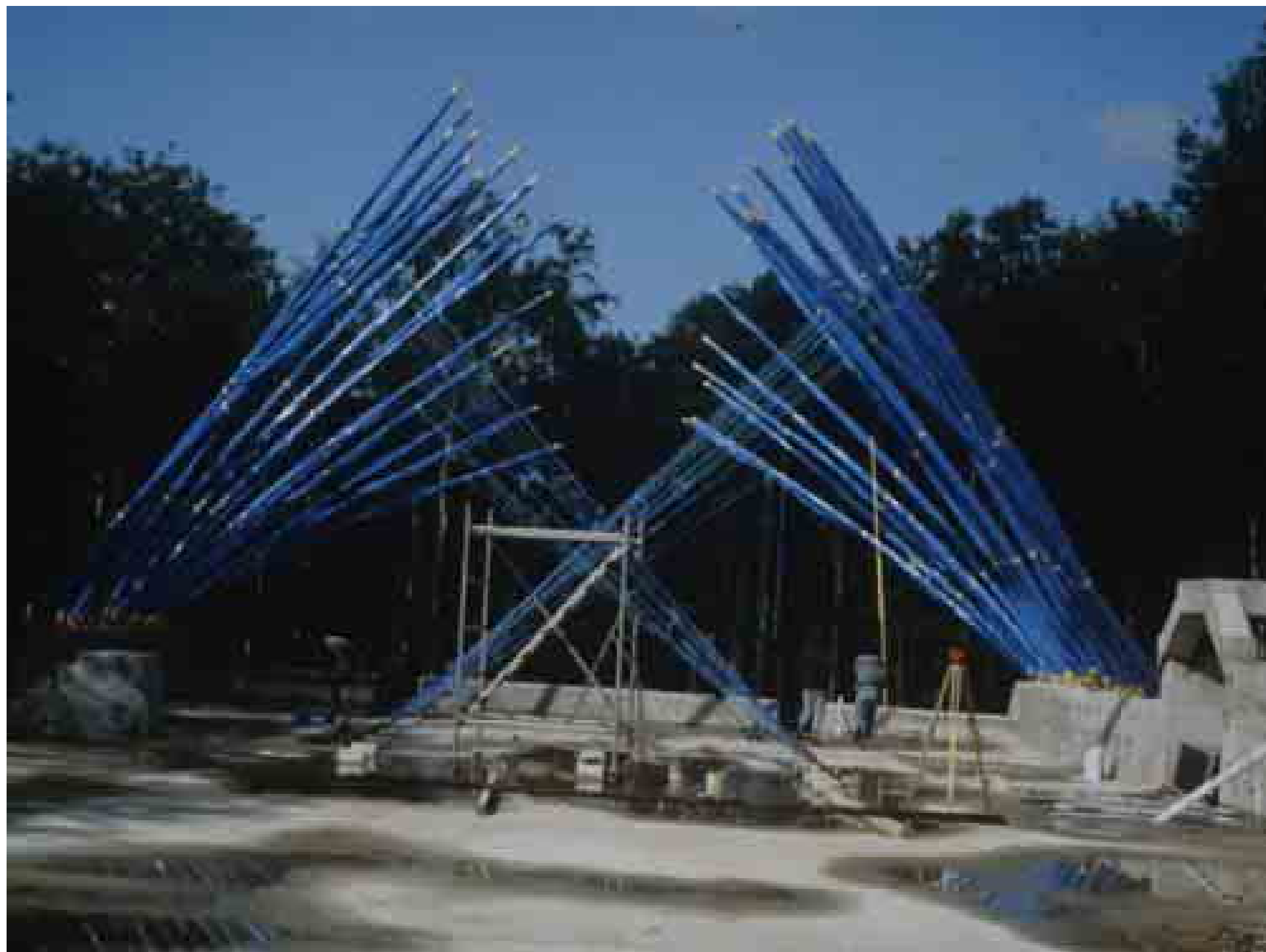
Jointing





workshop long section







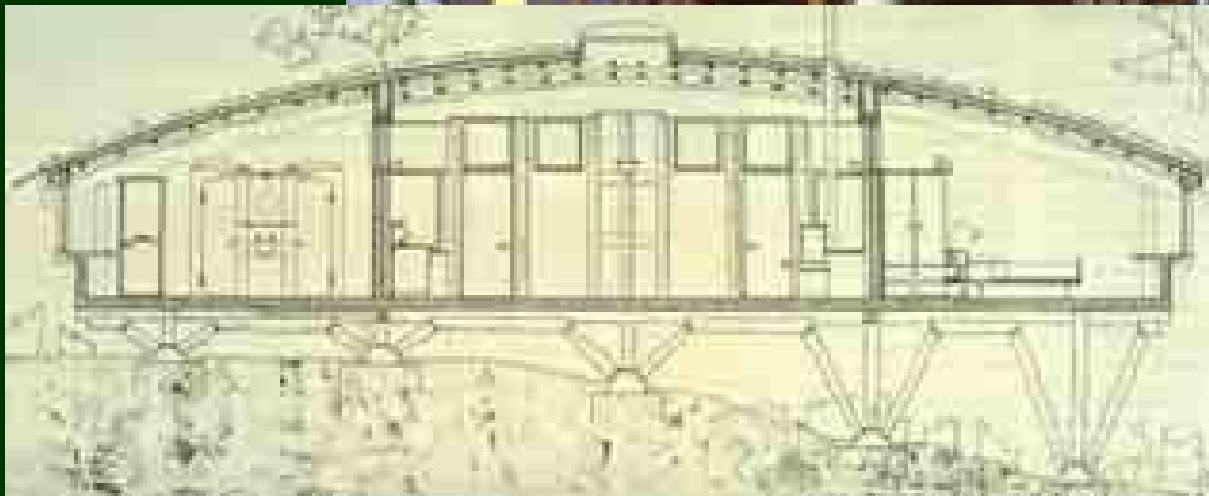
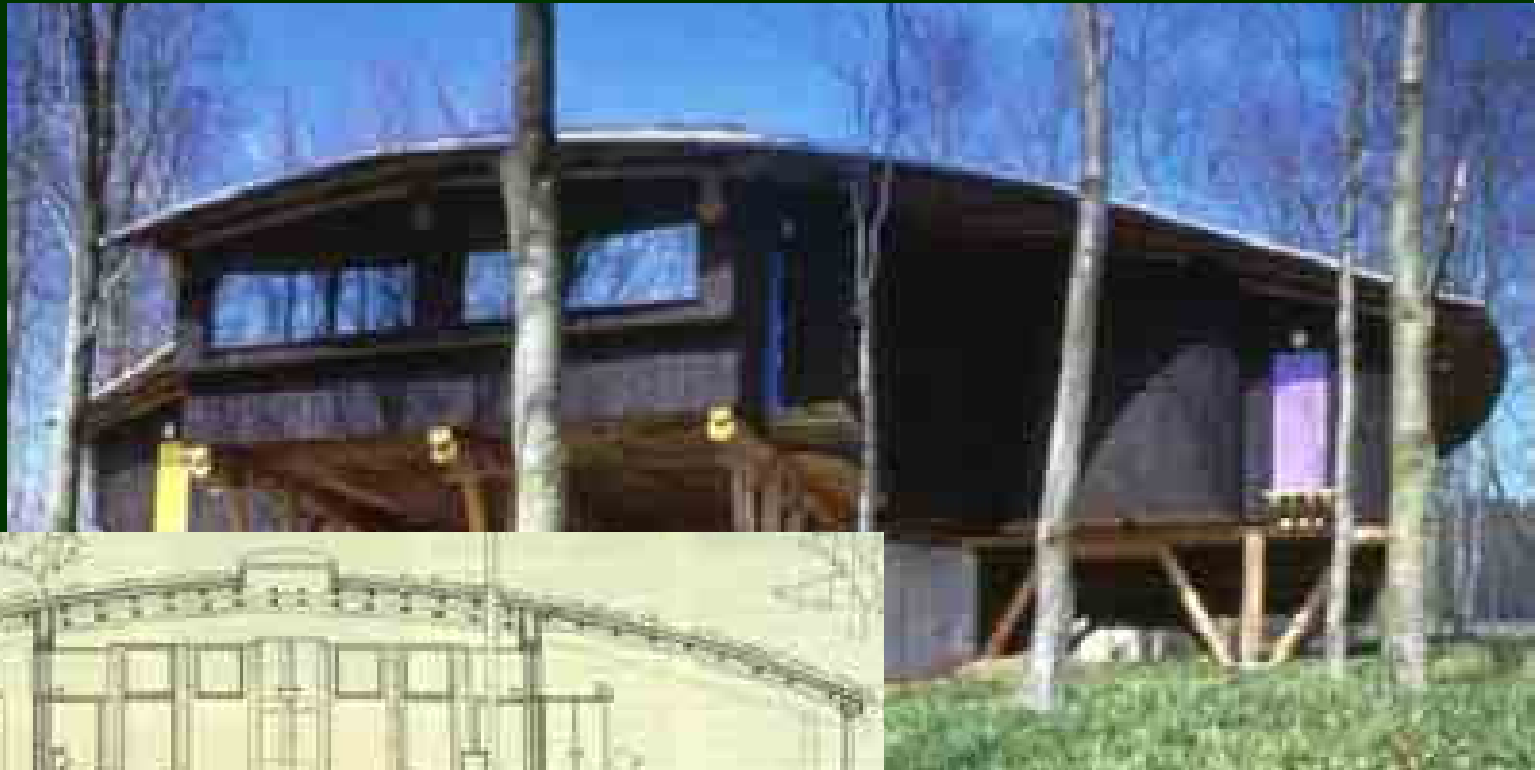


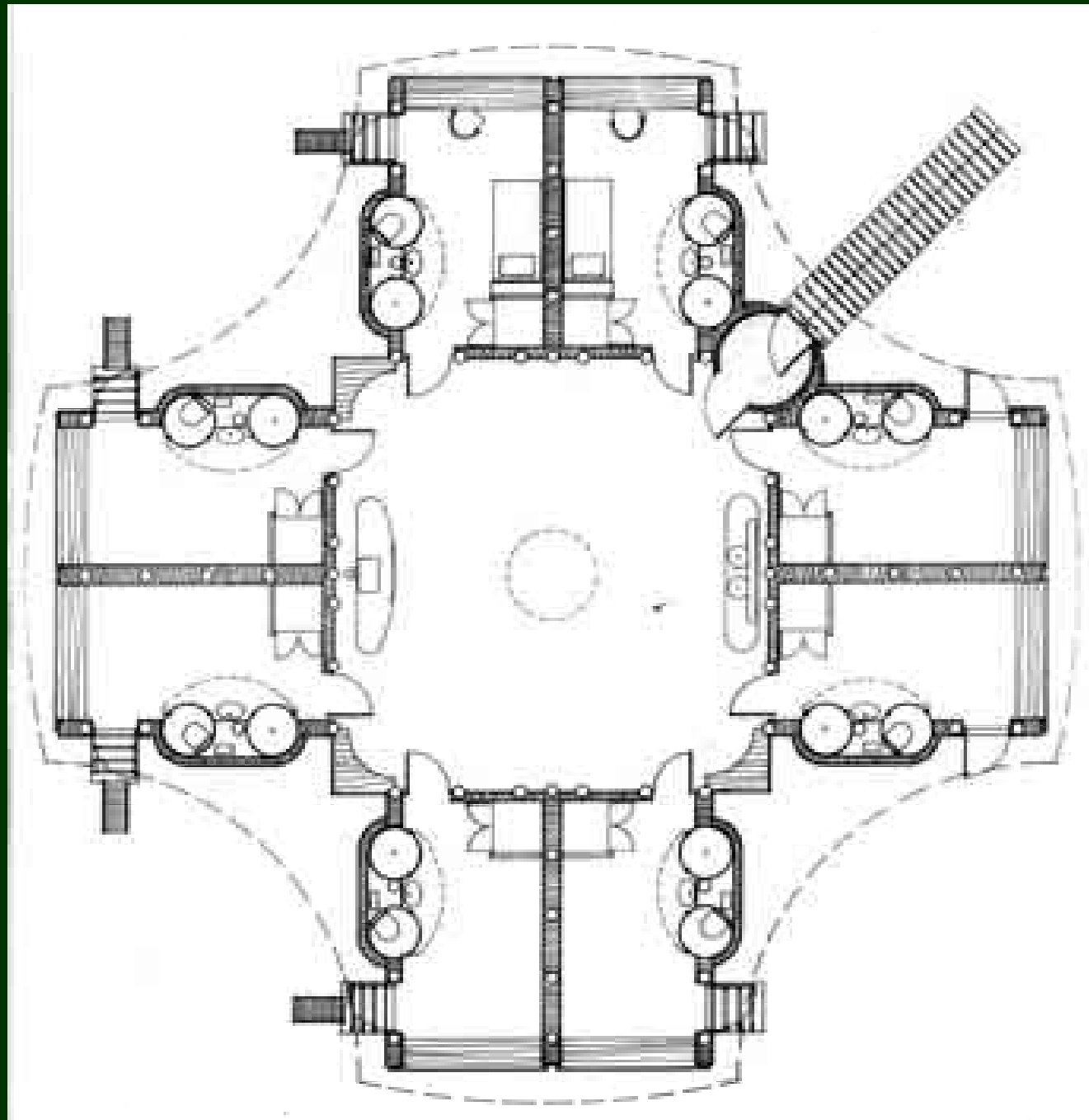


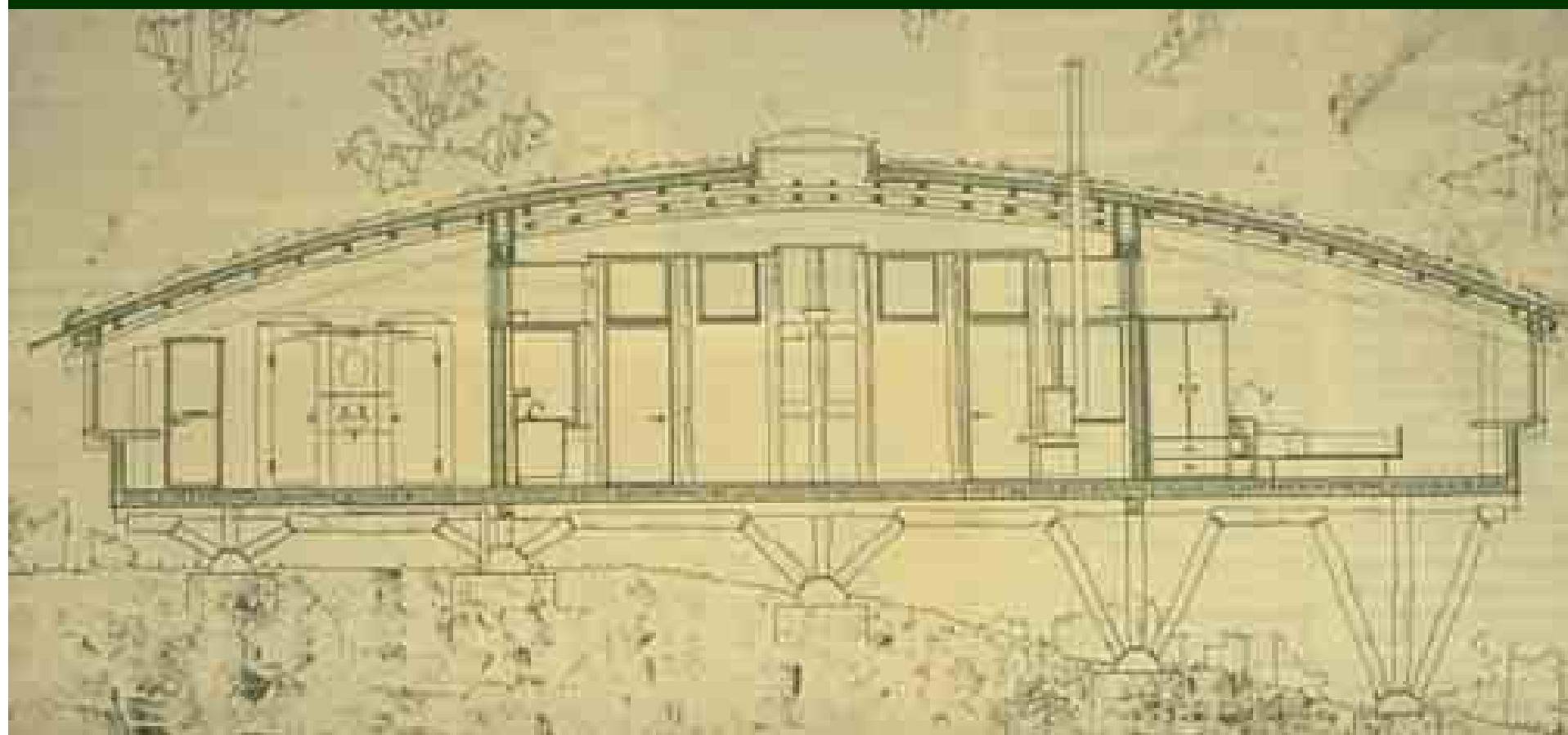
Hooke Park College, Dorset

- Westminster Lodge

1996



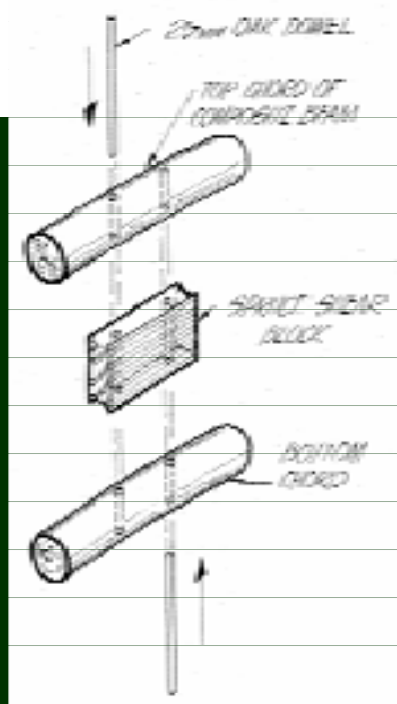
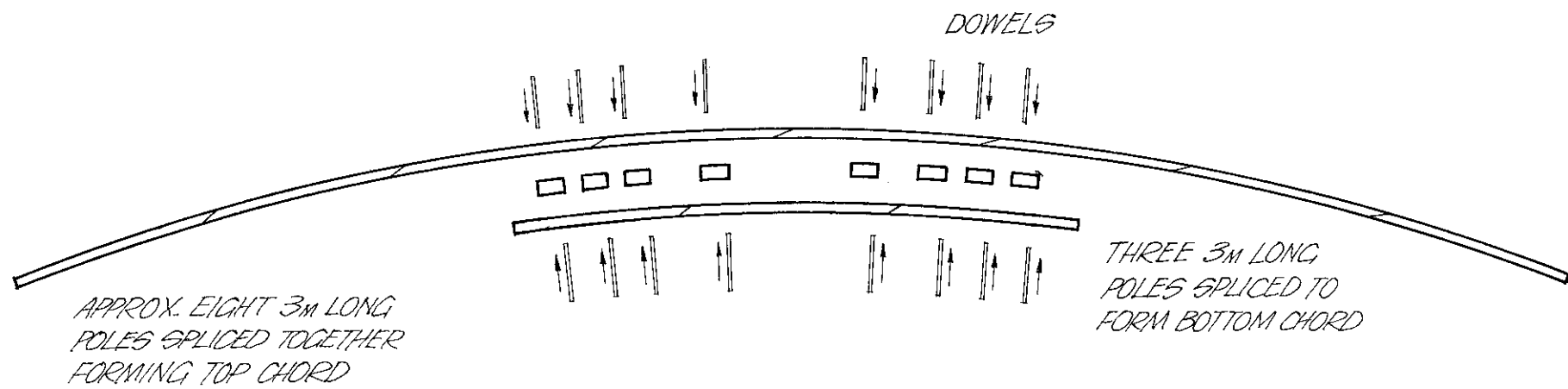




Model making











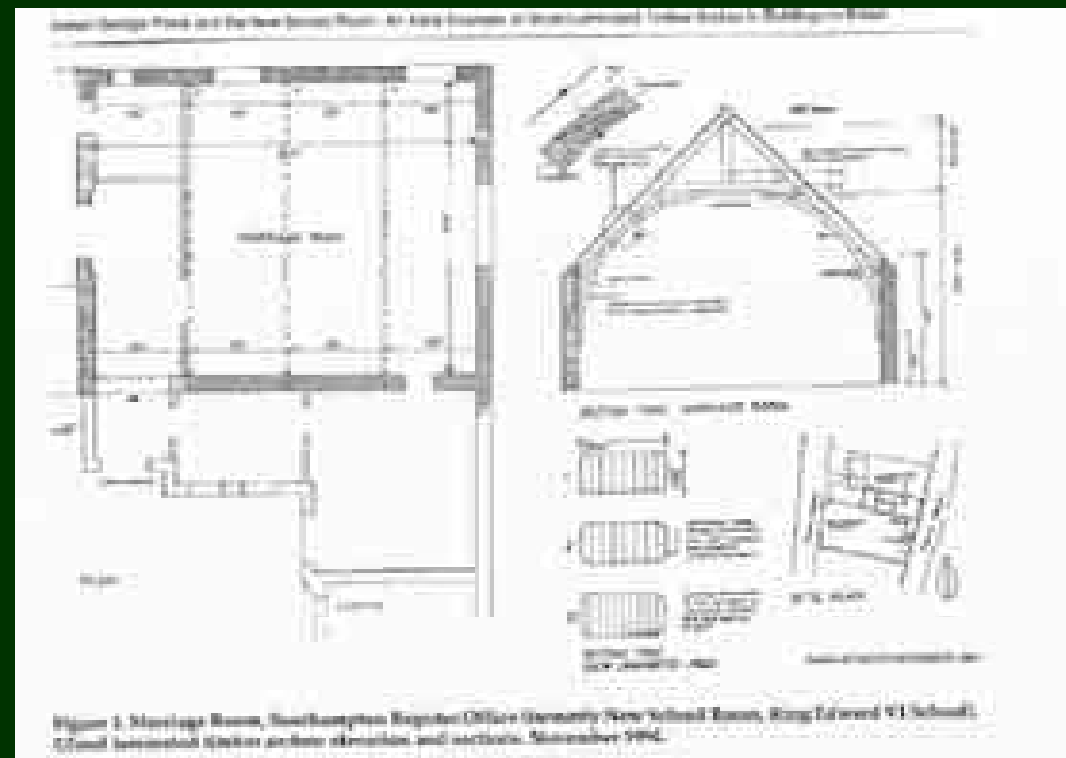




Glulam

a historic material





Opened August 1860









Waterloo Entrance to the Festival of Britain - 1951



Glulam – a modern material



Sheffield Winter Gardens

Sheffield Winter Garden

Architect:
Pringle Richards Sharrat

Engineer:
Buro Happold

Timber Engineering contractor
Merk Holzbau GmbH & Co KG



Sheffield Winter Garden

The idea:

**To design Gateway Building
for Urban Regeneration**

Sheffield Winter Garden

The challenge:

To design a building to inspire

To design a building for public enjoyment

Sheffield Winter Garden

The solution:

A natural environment

Wood used as a modern material

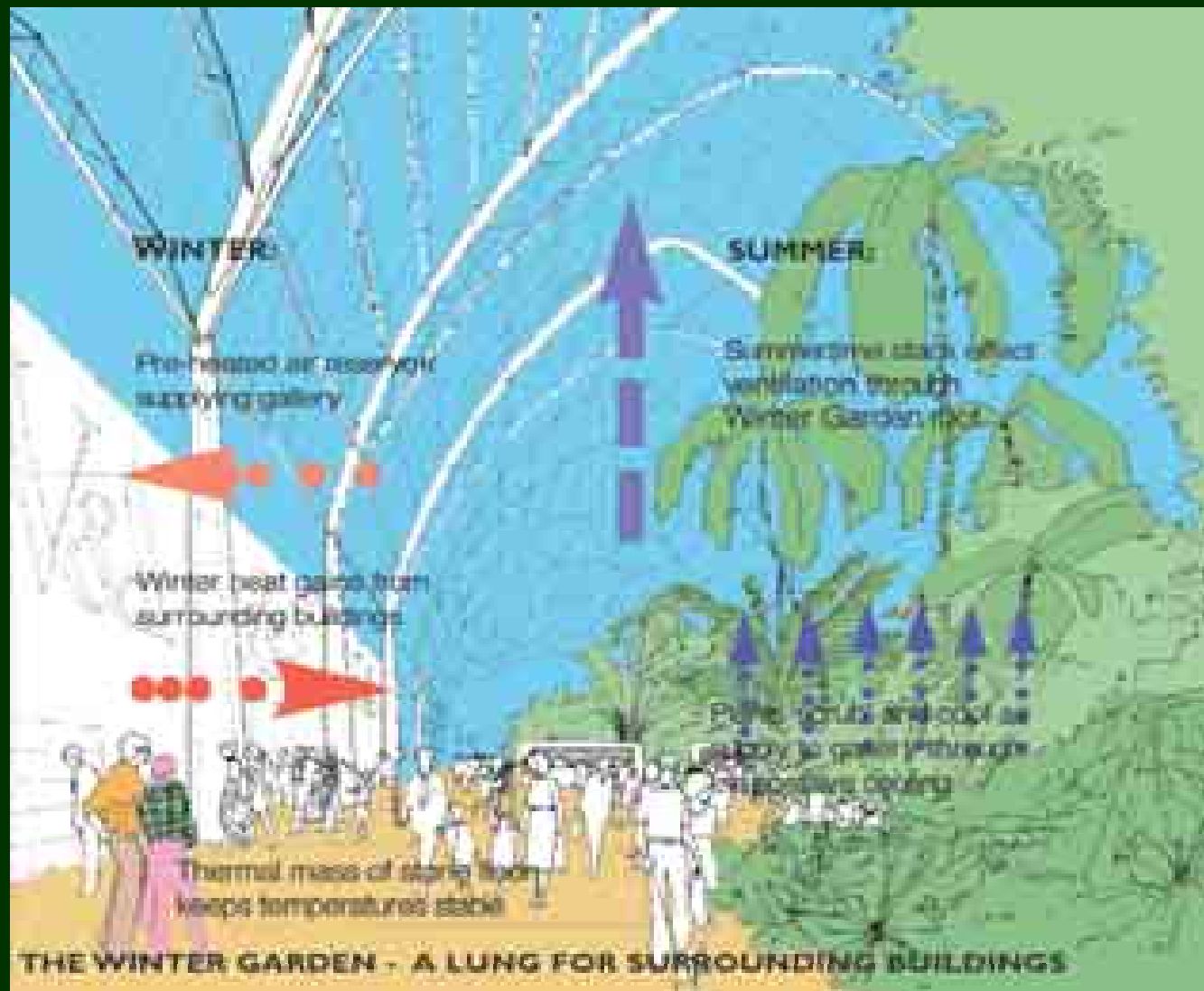
Sheffield Regeneration



Heart of the City



Winter Garden: Design Considerations



Common Name	Strength Class	Durability Class	Mean Stiffness N/mm²	Density range and Mean	Relative Cost
European Oak	D30 – D40	Durable	10,500 - 13,500	670-710-760	High
European Larch	C16 – C24	Moderately Durable	9,000 - 10,500	470-600-650	Medium
Douglas Fir <i>N. American</i>	C16 – C24	Moderately Durable	10,000 - 11,000	510-530-550	Medium
Redwood / Scots Pine	C14 – C24	Slightly Durable	9,000 – 10,500	500-520-540	Low
Douglas Fir <i>UK grown</i>	C14 – C18	Slightly Durable	9,500 – 11,000	470-510-520	Medium
European Whitewood (Silver Fir/ Norway Spruce)	C16 – C24	Slightly Durable	8,800 – 10,800	440-460-470	Low
Sitka Spruce (UK Sitka)	C14 – C18	Not durable	6,500 – 8,000	400-440-450	Low

The Structure

75m long; 20m high; 22m span

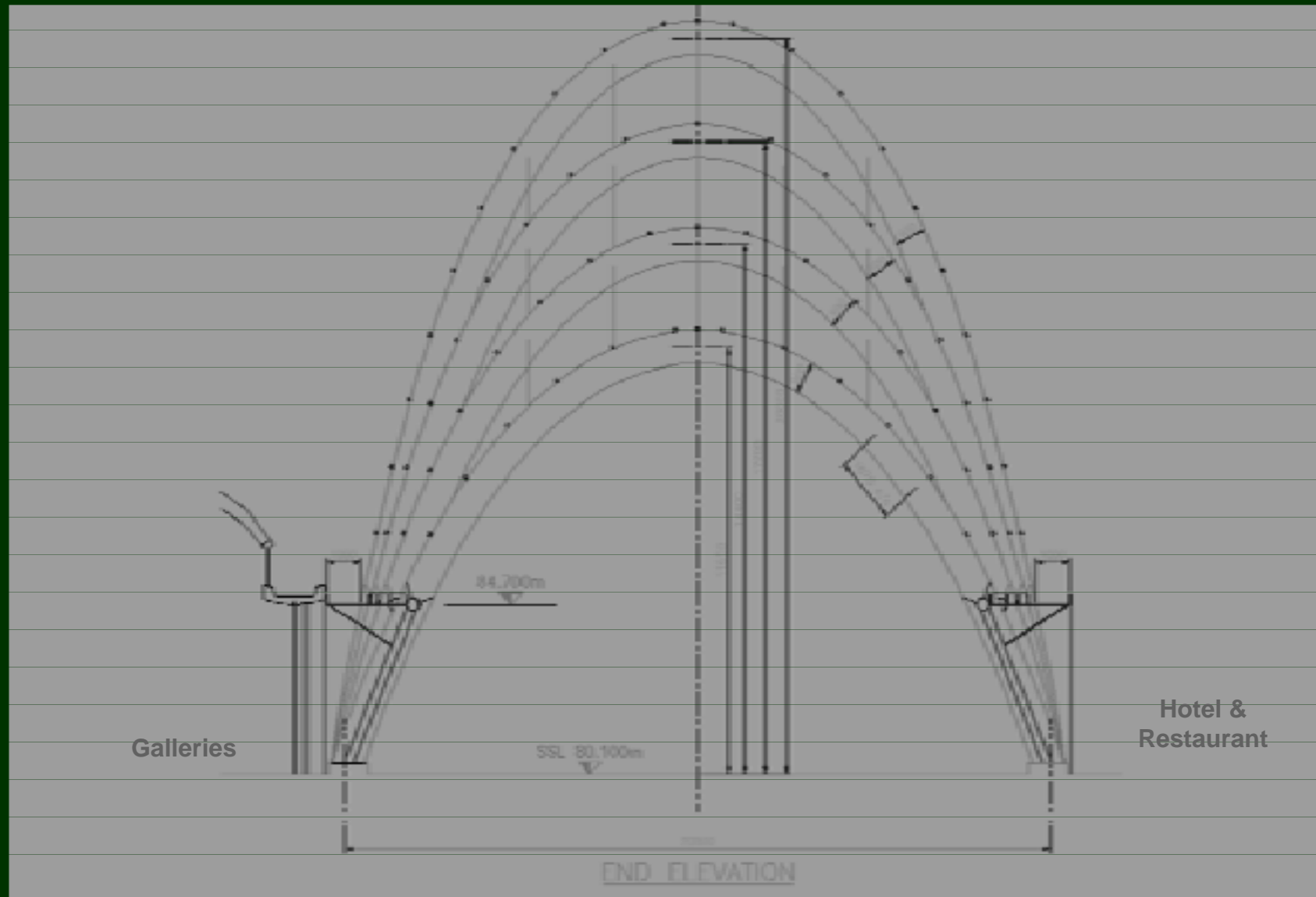
The principal structural element sizes are:

- Arches - 210mm wide x 910mm deep**
- Purlins - 150mm wide x 225mm deep**
- Raking Struts – 245 mm diameter**

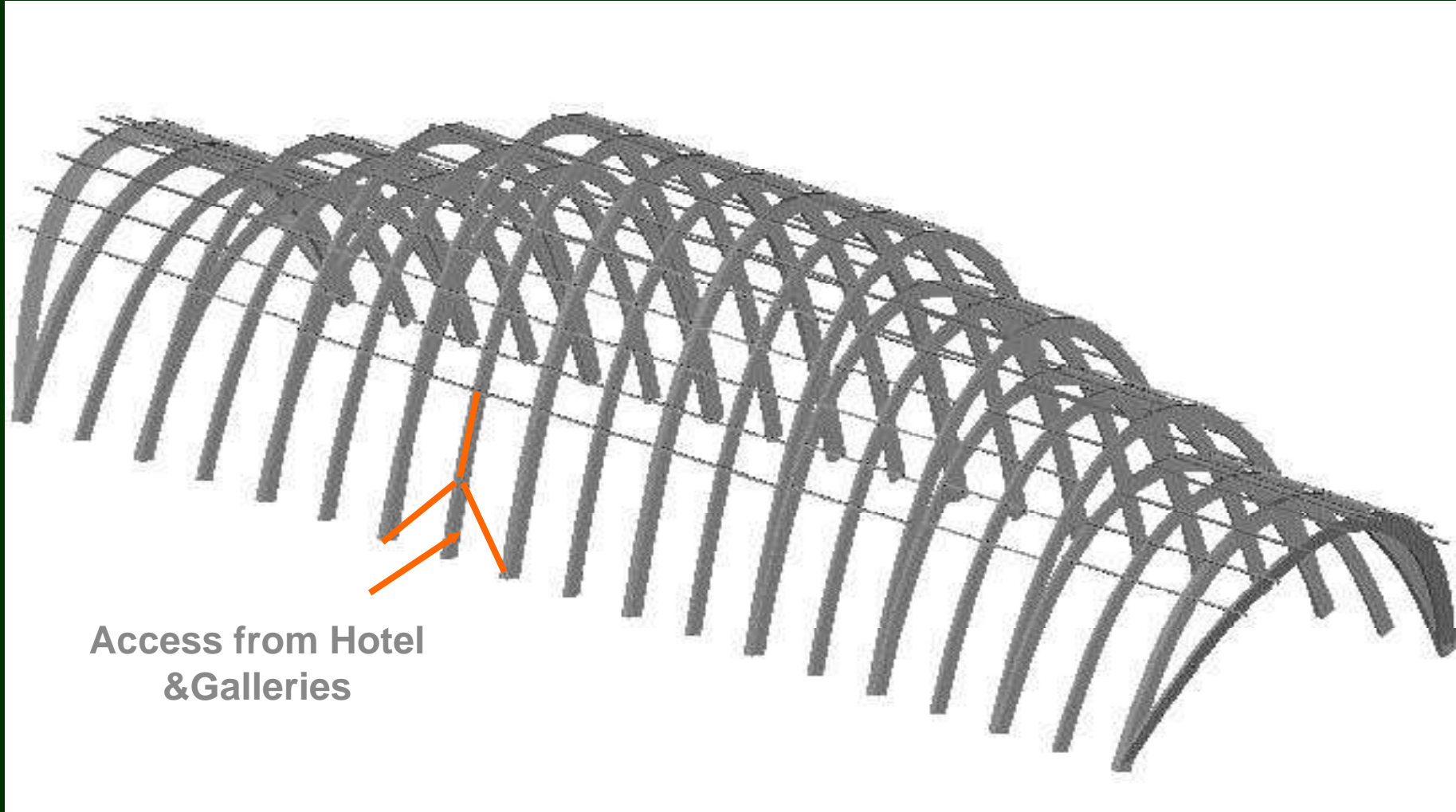
All timber is Polish Larch to grade GL28. Glulam manufactured by Derix and fabricated by Merk, in Germany .

The steelwork is mild steel, galvanised to avoid staining the wood.

Arch Geometry – arches at 3.75 metre spacing



Structure



Superstructure



Superstructure

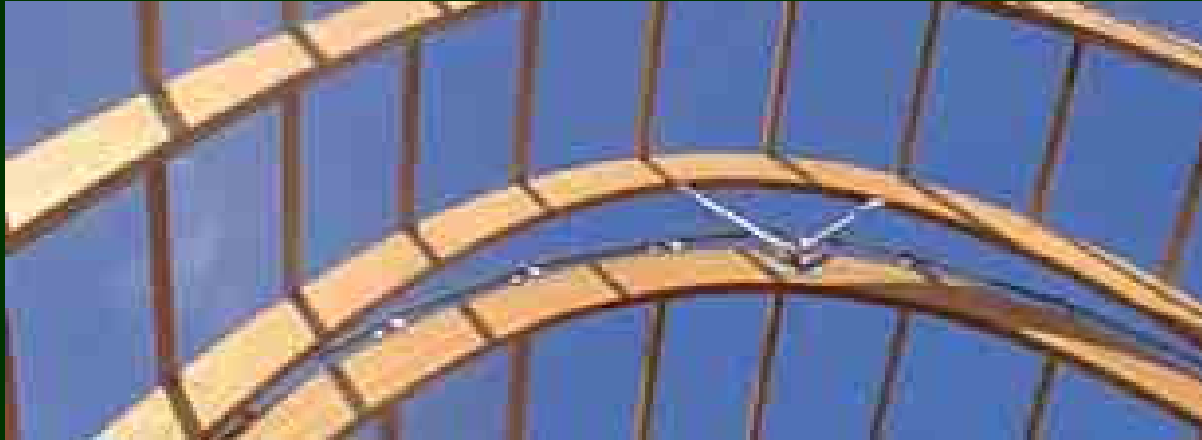


Superstructure



Details:

Arch Apex



Finished Building



Details:

Base









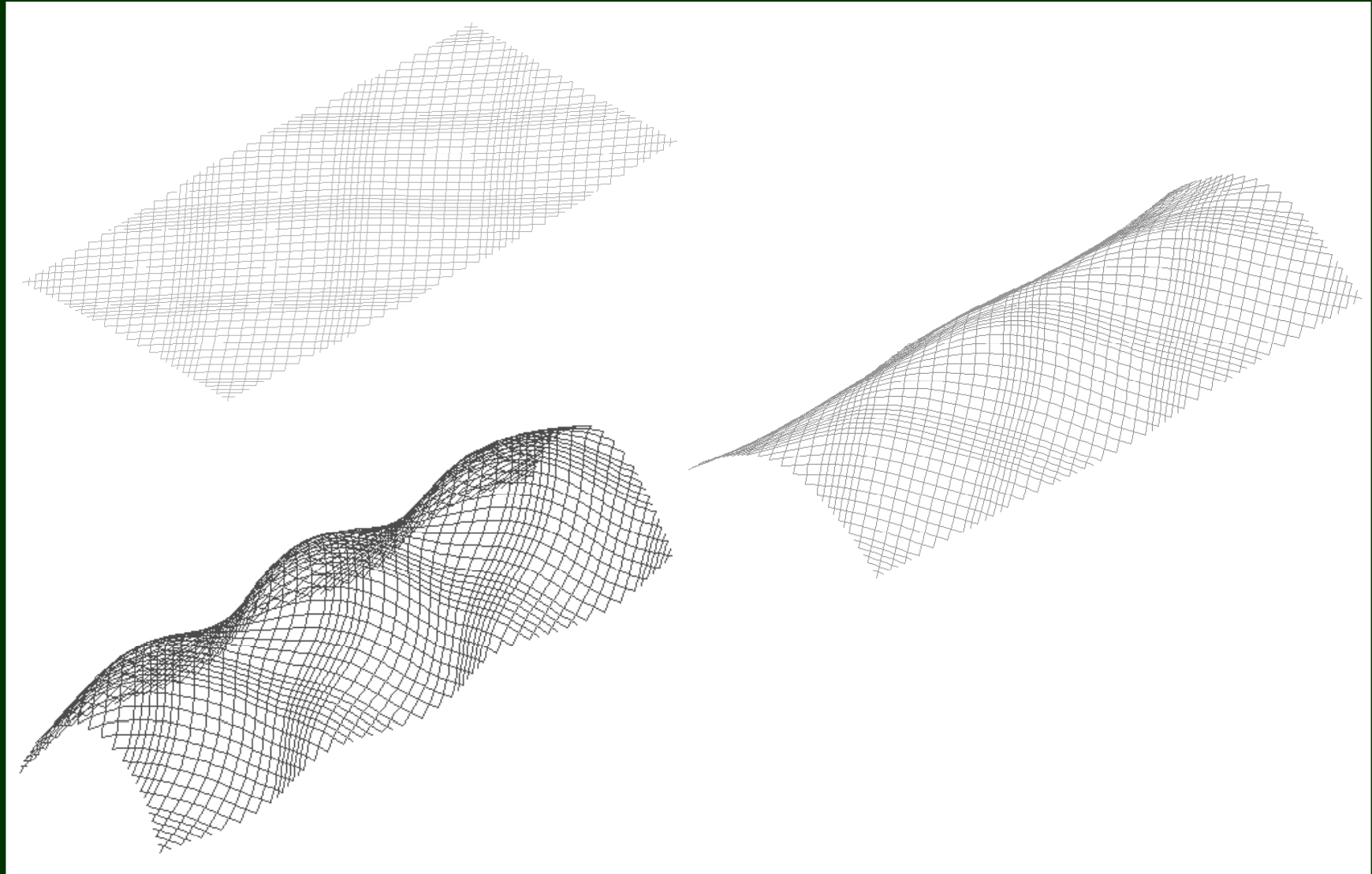
Timber Gridshell

sophisticated structures

Timber Gridshell Construction

The idea:

Timber Gridshell Construction – the principle



Gridshell precedents

Gridshell	Span	No of Layers	Lath size	Material	Bracing
Mannheim	60m x 60m	4	50mm x 50mm at 0.5 m	Hemlock	Twin 6mm cables
Japan Pavilion	72m x 35m	2	120mm rad at 1.0m	Cardboard tube	Glulam ladders
Earth Centre	6 x 6m	2	32mm x 15mm at 0.4m	Oak	Twin 2mm cables
Downland Gridshell	48m x 15m	4	50mm x 35 mm at 1.0m	Oak	Timber cladding rails
Savill Garden	90m x 25m	4	80mm x 50mm at 1.0m	Larch	12mm birch plywood
Chiddingstone Castle	12m x 5m	4	40mm x 30mm at 1.0m	Sweet Chestnut	Twin 4mm cables

Gridshell Precedents



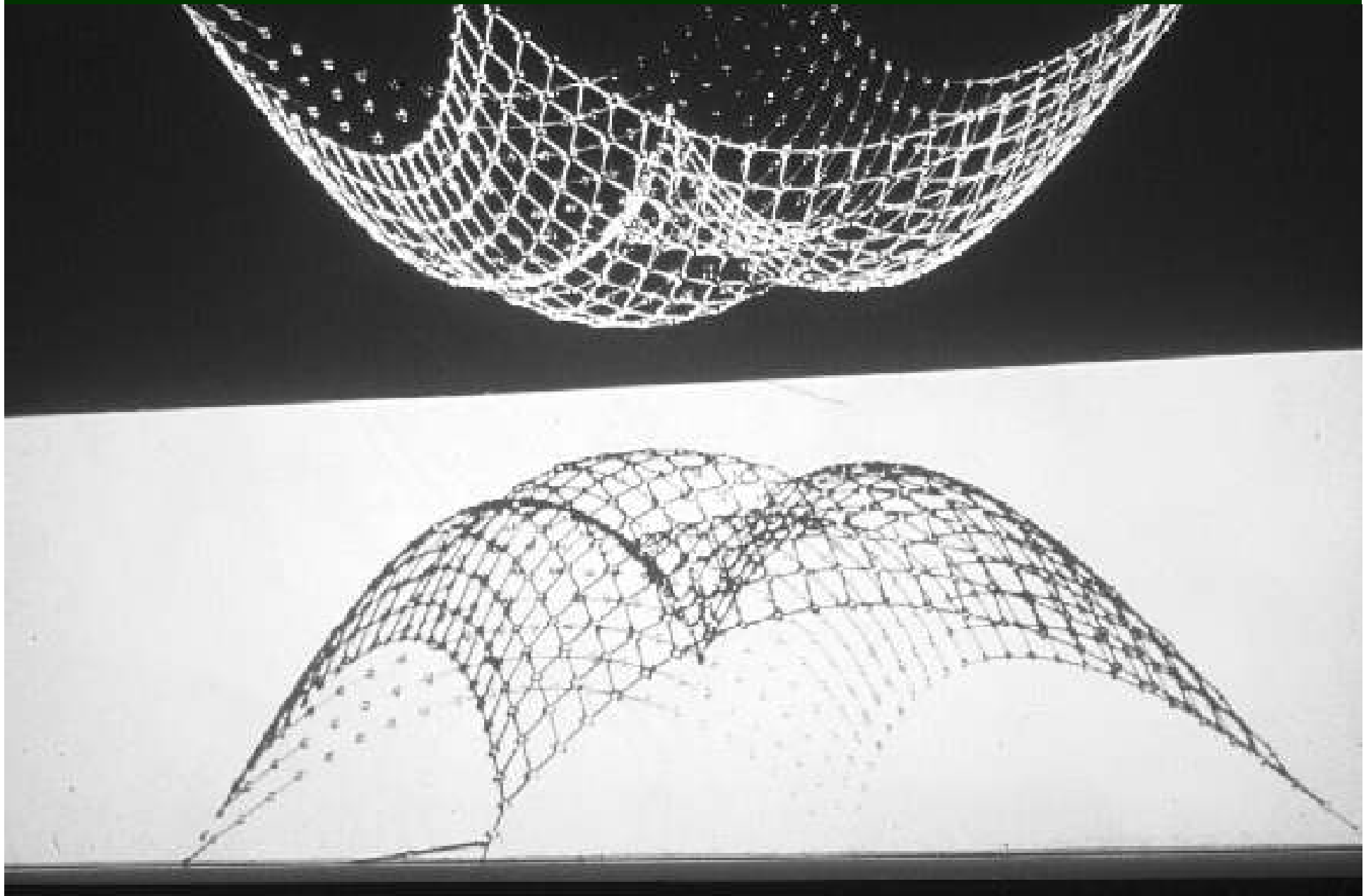
Mannheim Bundesgartenschau



50m span
4 Layers
50 x 50 hemlock

Design Team: Frei Otto / Ove Arup

Mannheim – a funicular structure

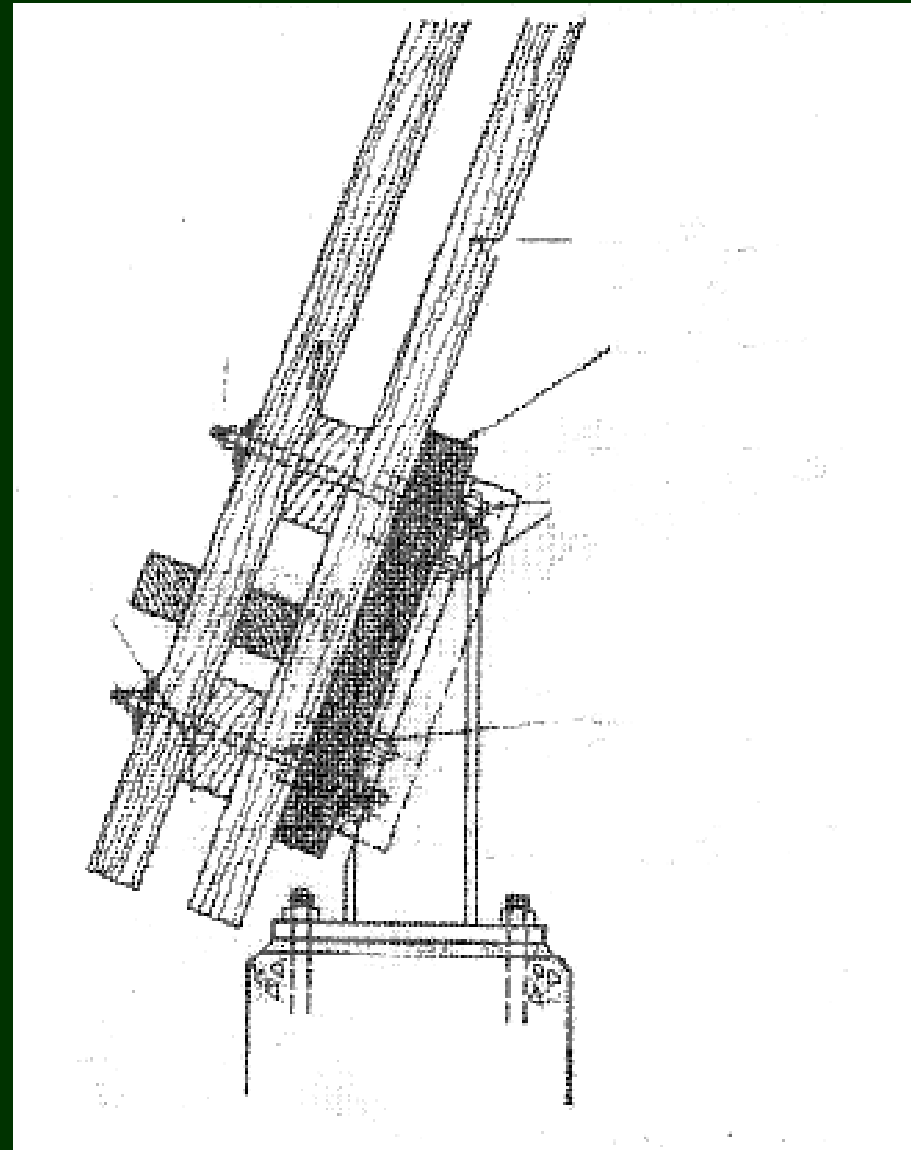




Mannheim Gridshell



Mannheim



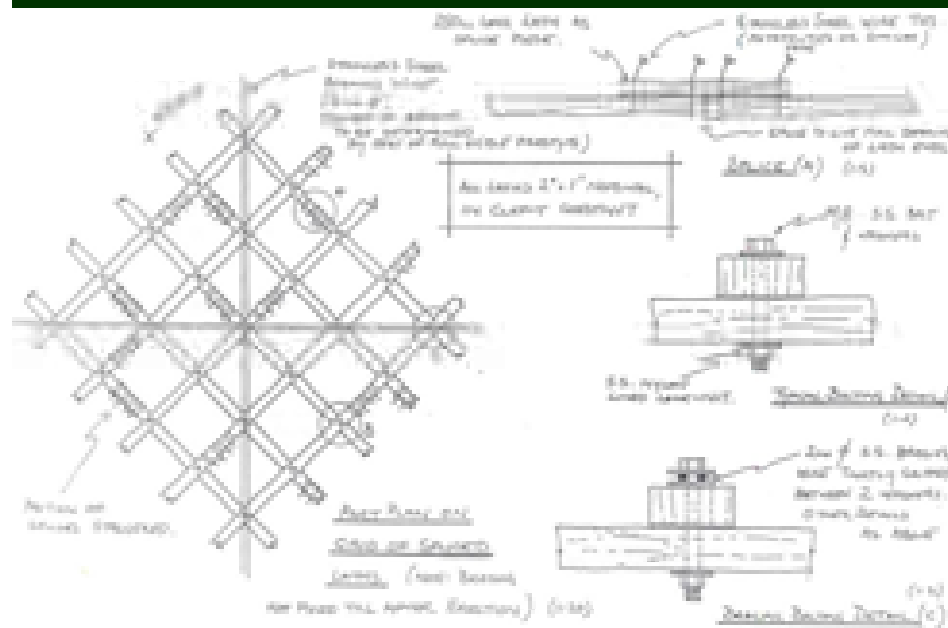
Earth Centre Doncaster

**6m span
2 Layers
32 x 15 oak**



Design Team: Grant Associates / Buro Happold

Earth Centre Gridshells

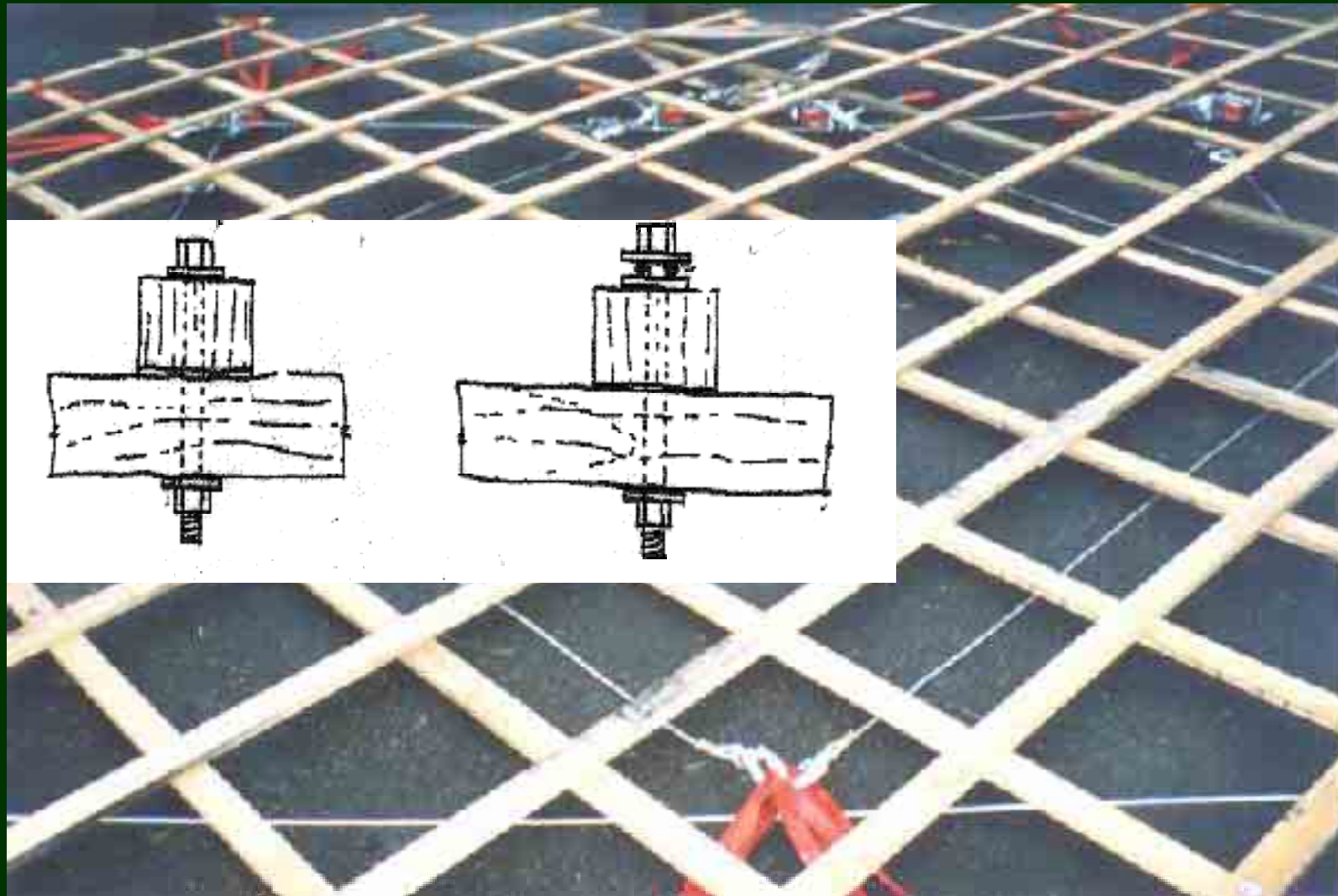




Earth Centre Gridshells



Earth Centre Gridshells



32mm x 15mm at 0.4m.

Bracing: twin 2 mm cables

Earth Centre Gridshells



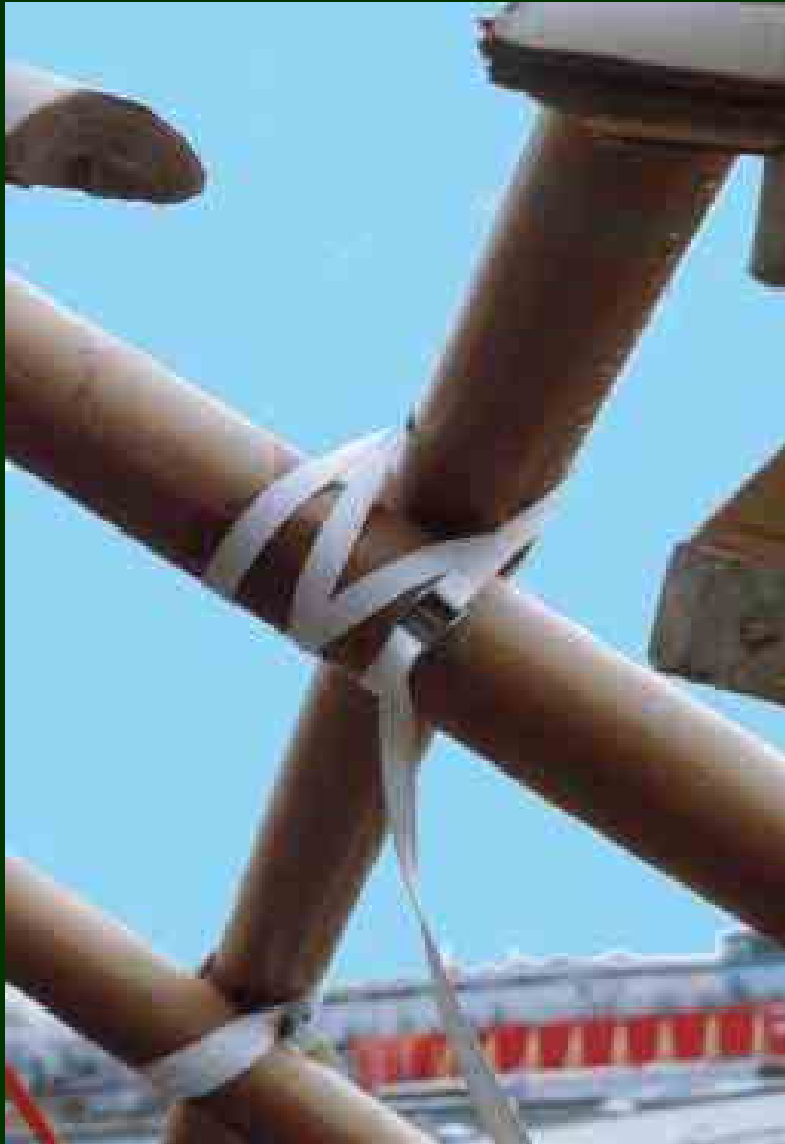
The Japan Pavilion Hanover EXPO 2000



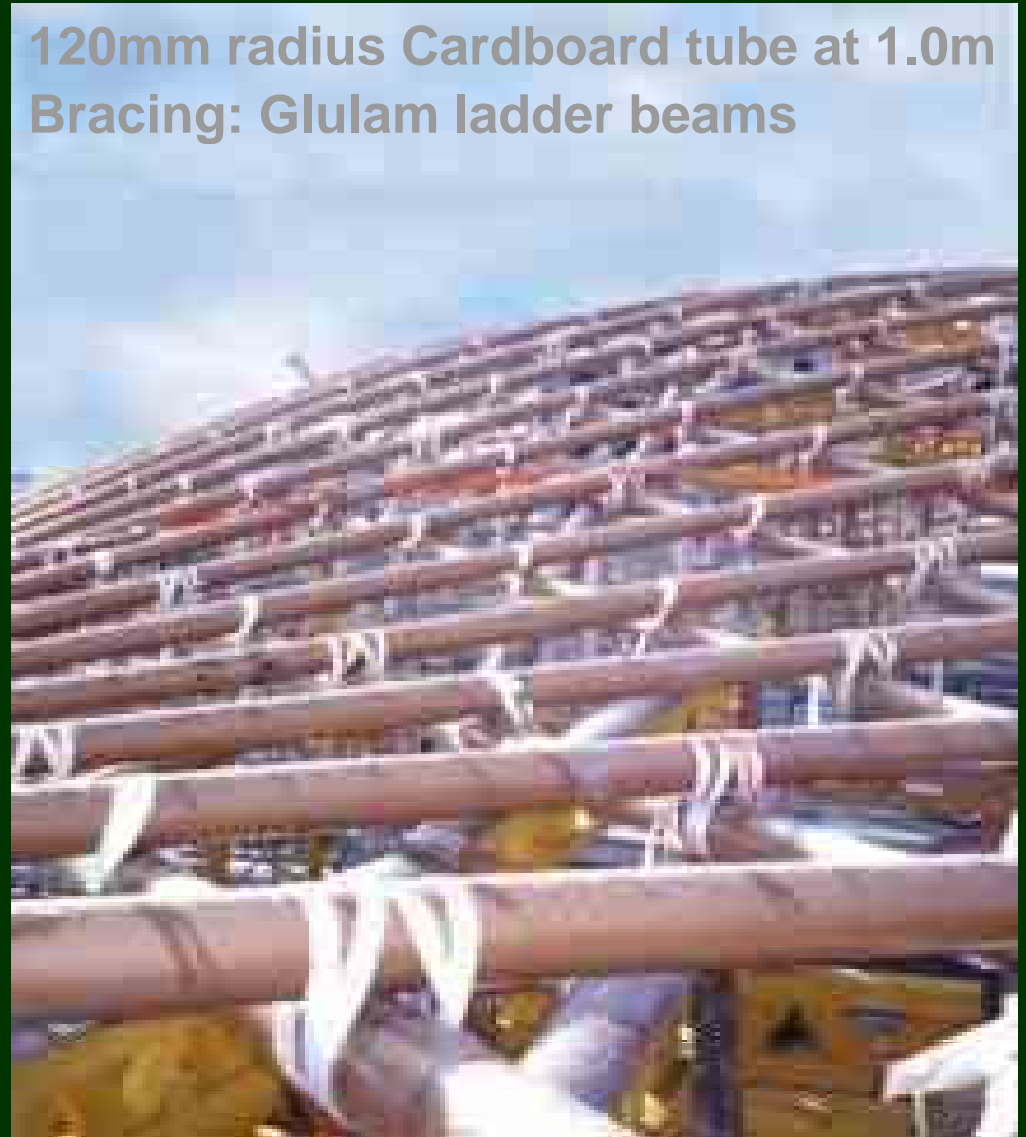
30m span
2 Layers
Cardboard Tubes

Design Team: Shigeru Ban/ Buro Happold

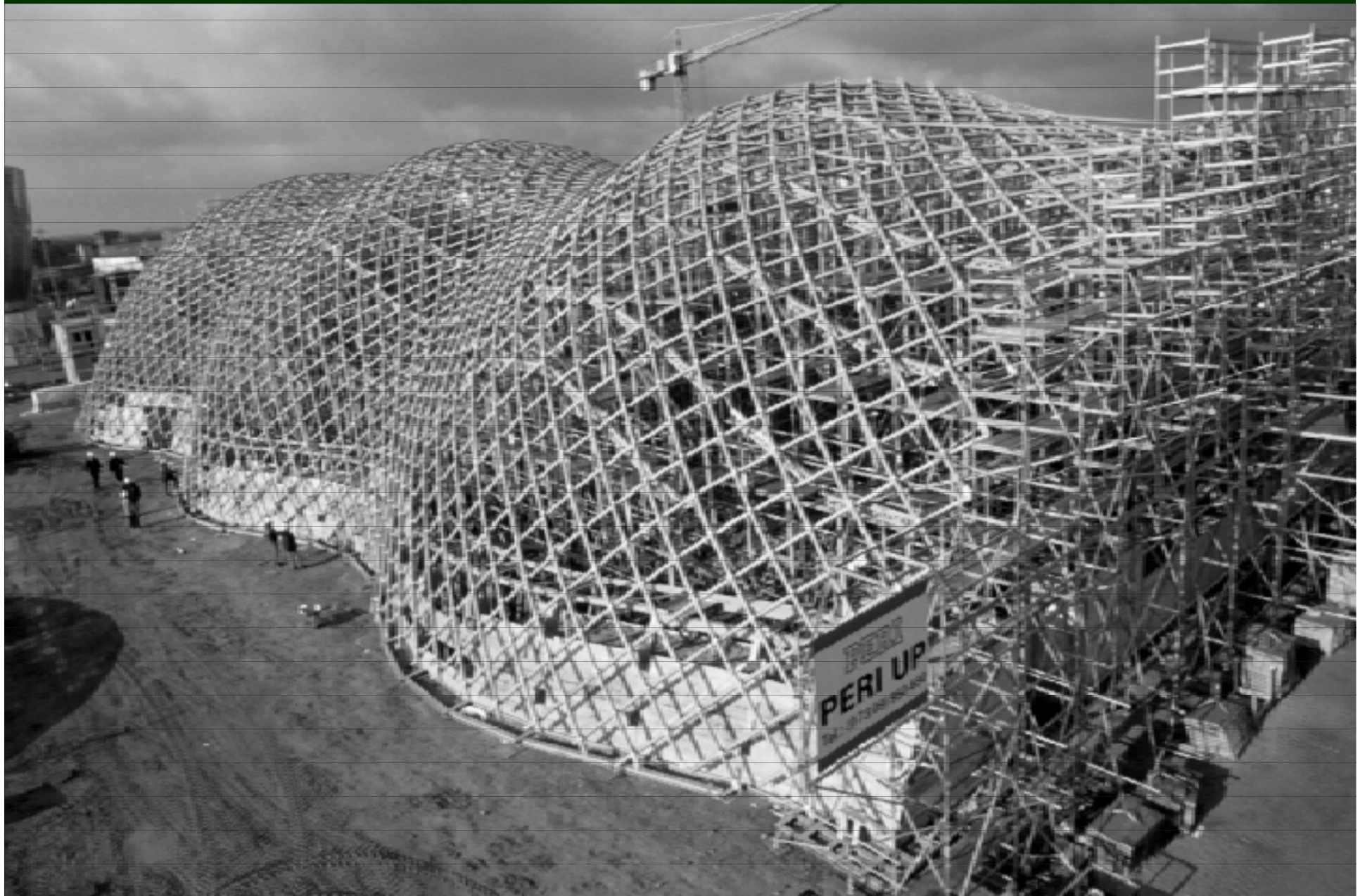
Japan Pavilion Hanover Expo 2000

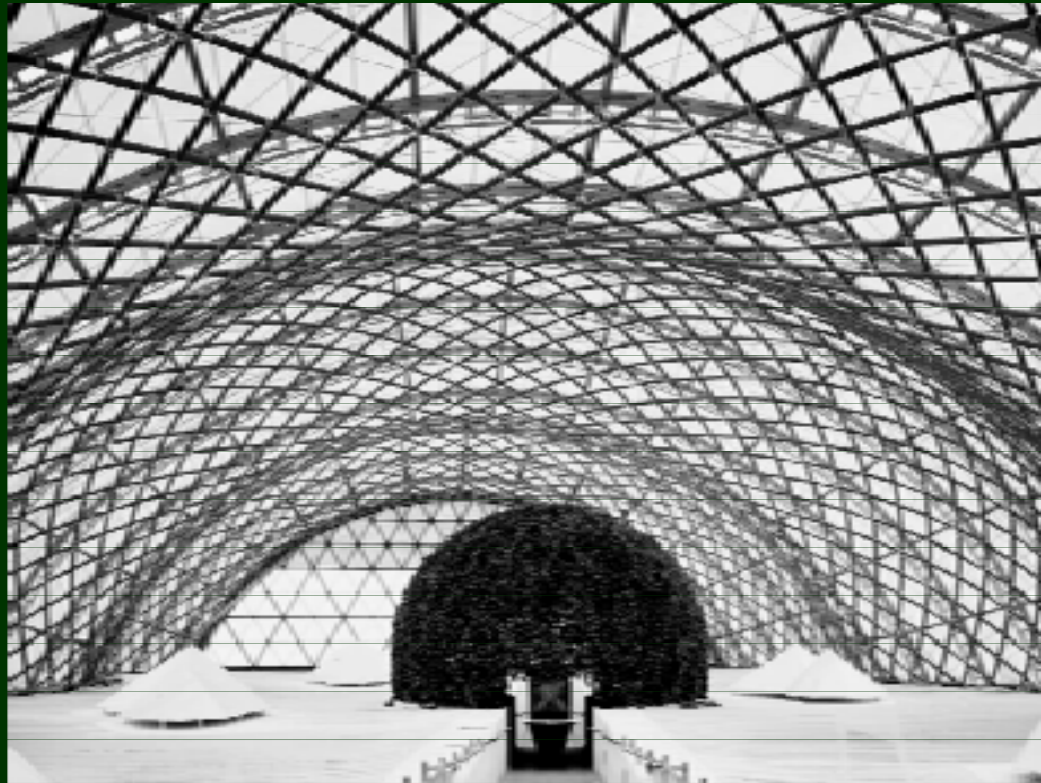


120mm radius Cardboard tube at 1.0m
Bracing: Glulam ladder beams



Japan Pavilion





**The Japan Pavilion
Hanover EXPO 2000**



Downland Gridshell



48m x 15 m
4 Layers
50mm x 35mm oak

Design Team: Edward Cullinan Architects/ Buro Happold



Downland Gridshell

The Client Brief:

To design modern building in a sensitive environment

To use an innovative design

Downland Gridshell

The complication:

**Re-discover the techniques used in 1975
at Mannheim**

Devise design methods

**Develop construction technique and
teach others**

**Maintain confidence of the Client and
design team**

Downland Gridshell

The solution:

Innovative design and method

Prototyping – model and full scale

Good communication



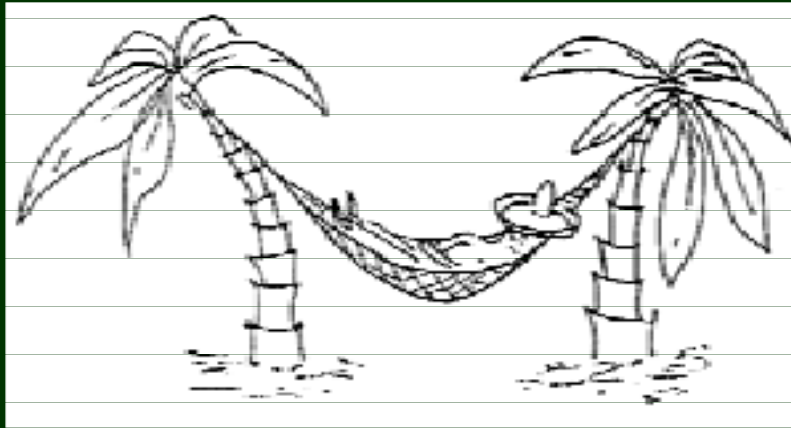




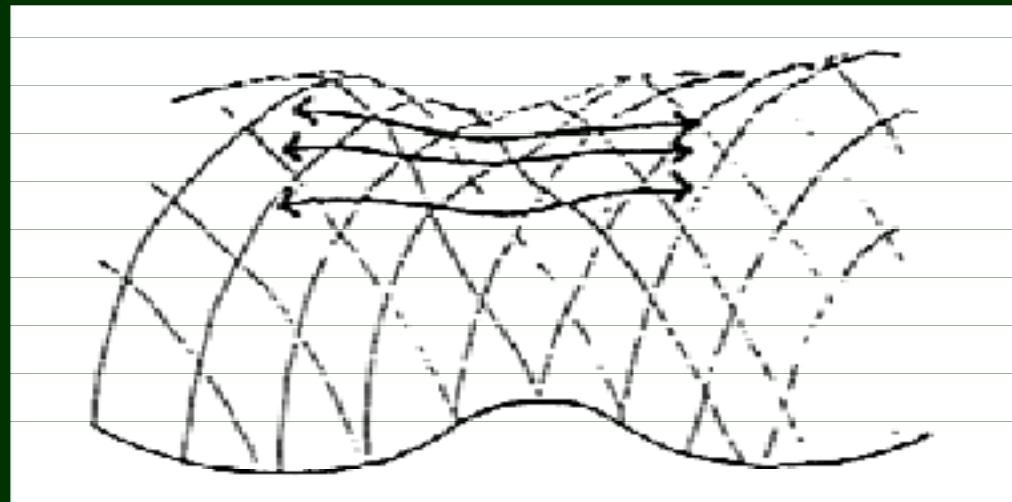




Structural principle



**Not a
funicular
Structure!**



Construction Method

Mannheim



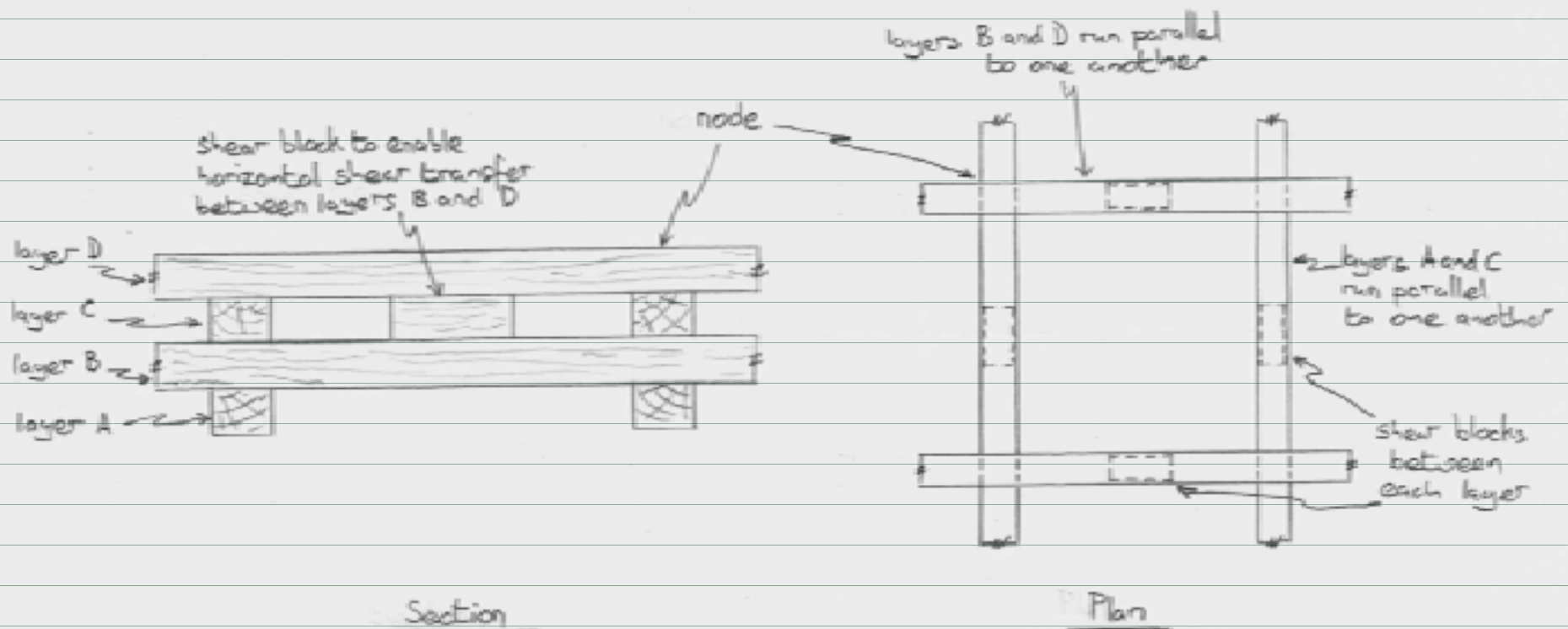


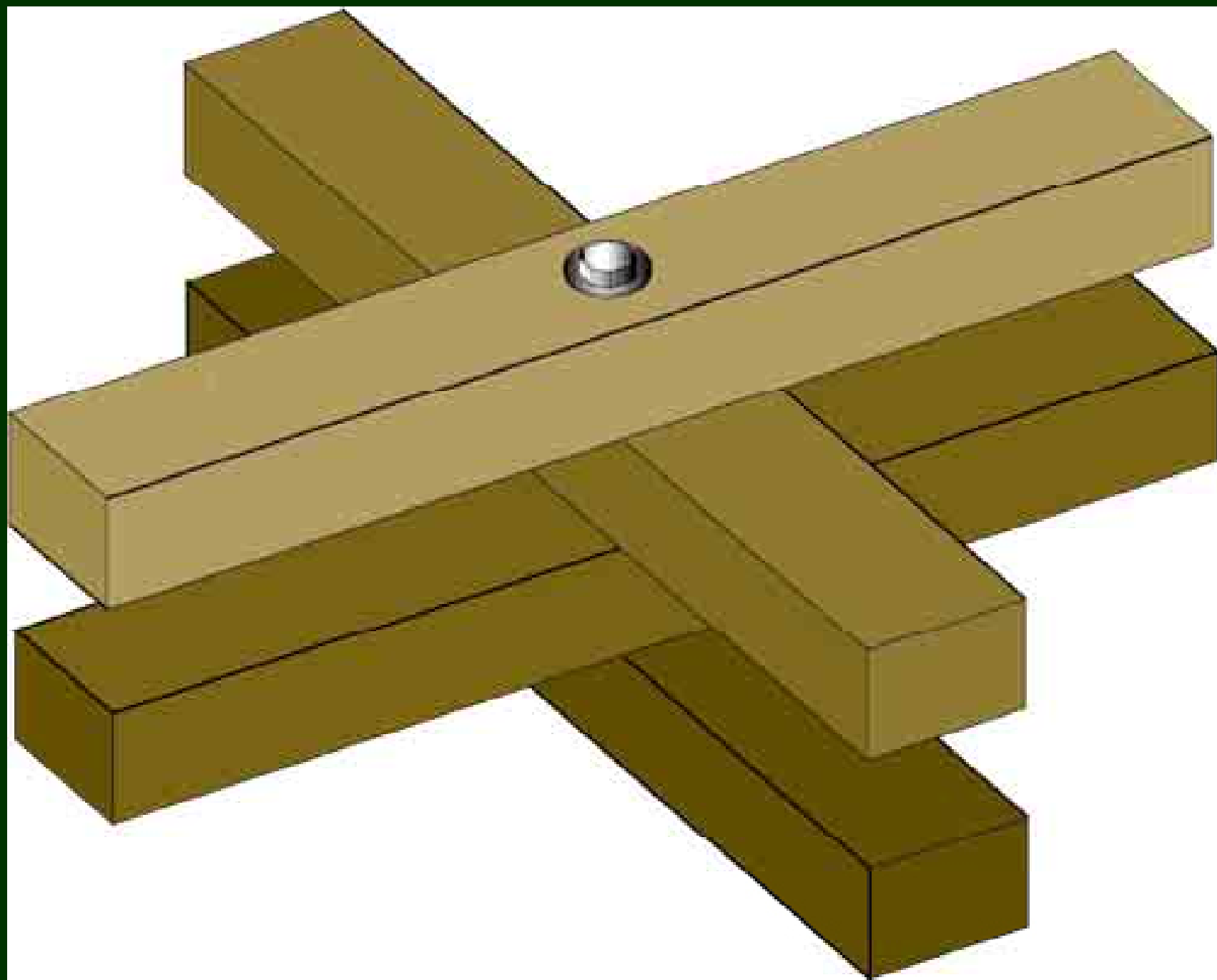


Japan Pavilion

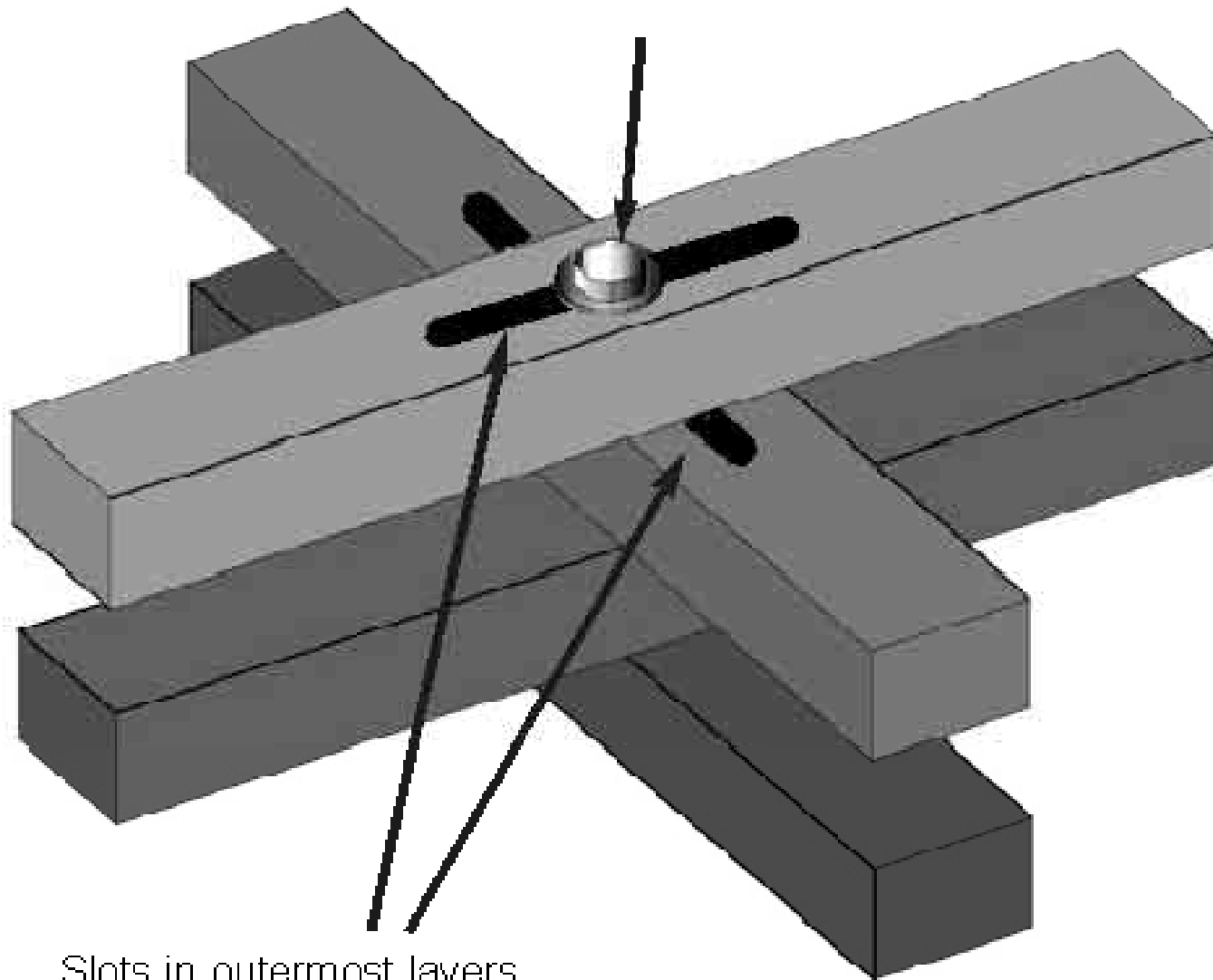




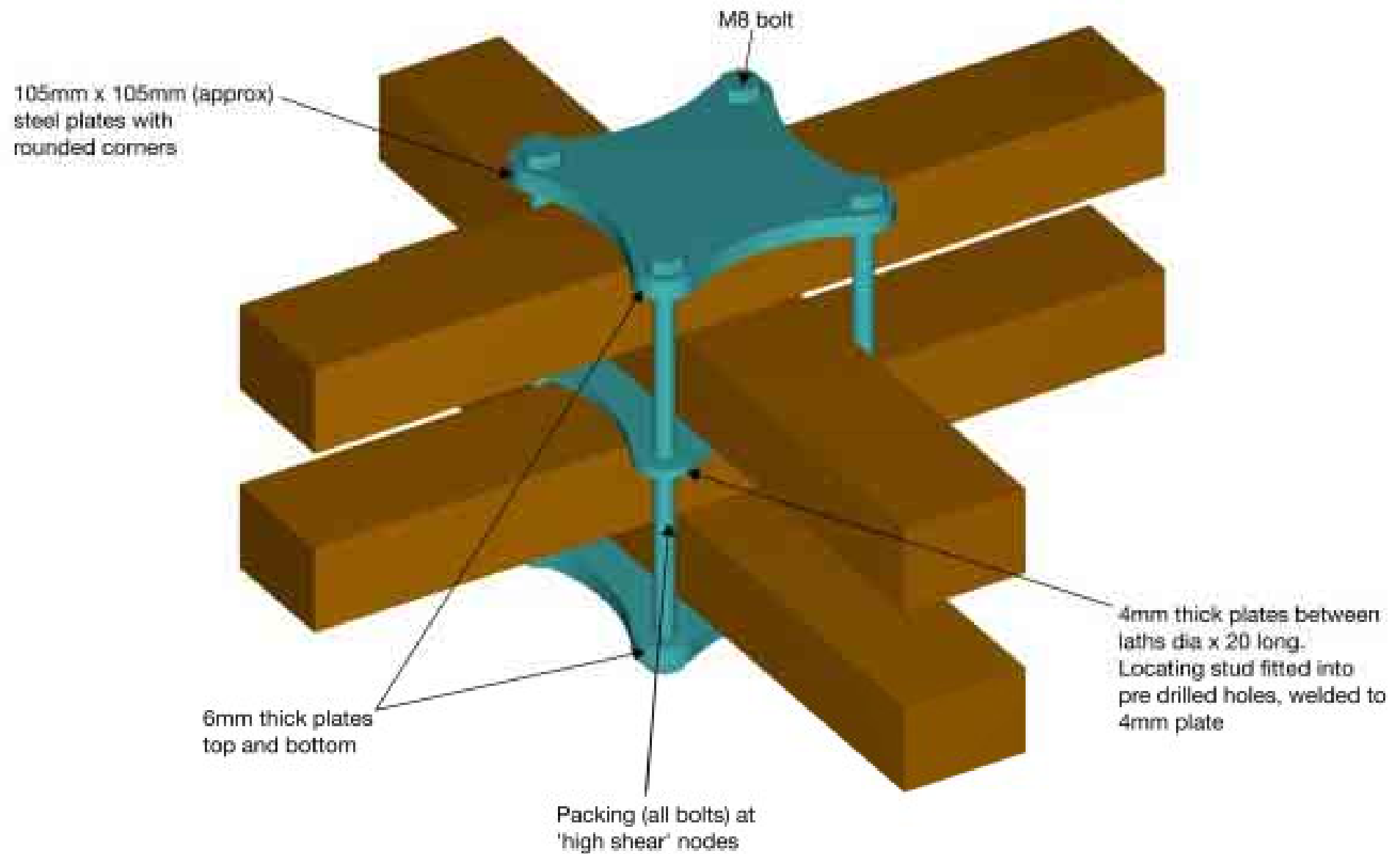


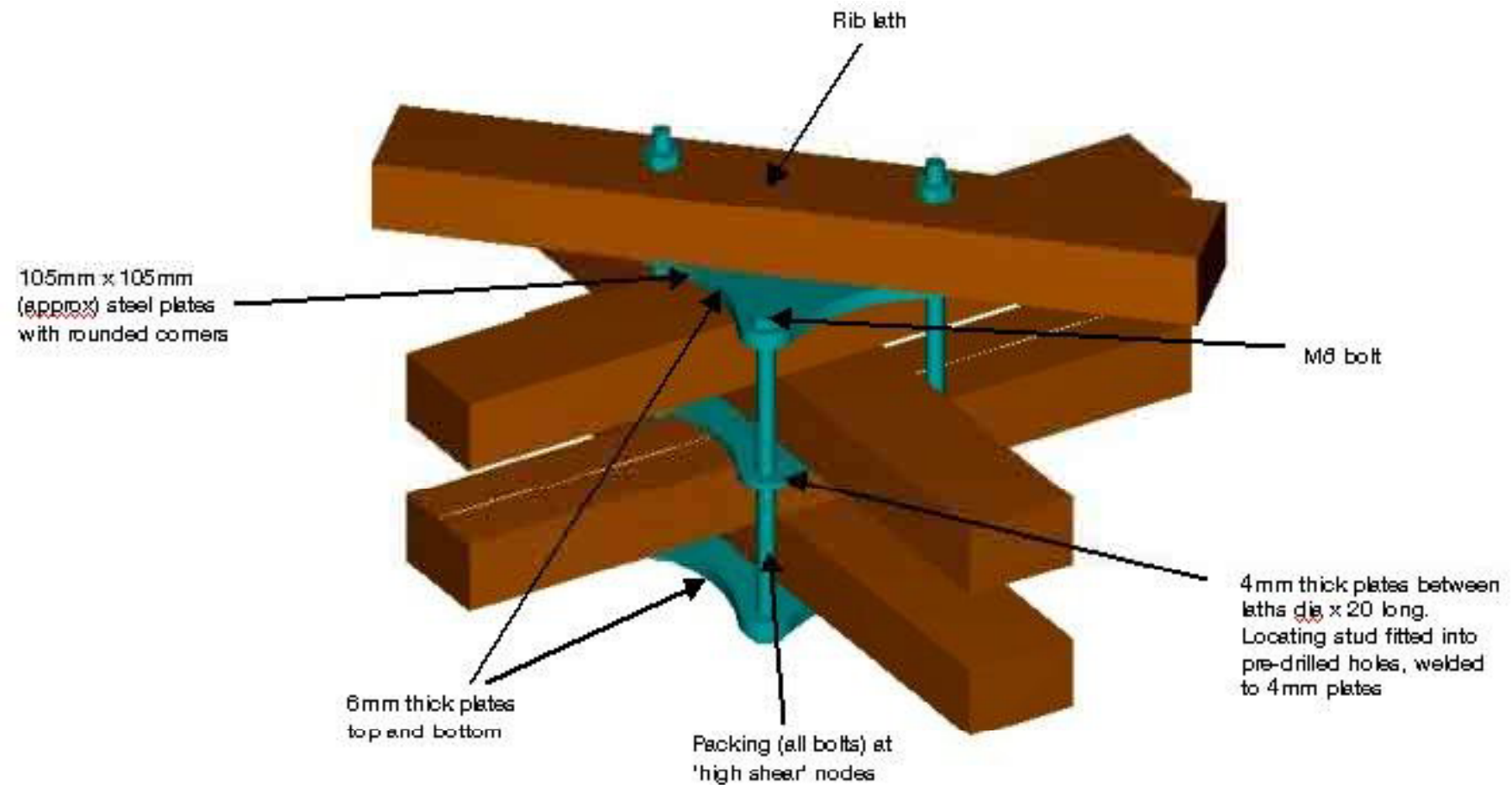


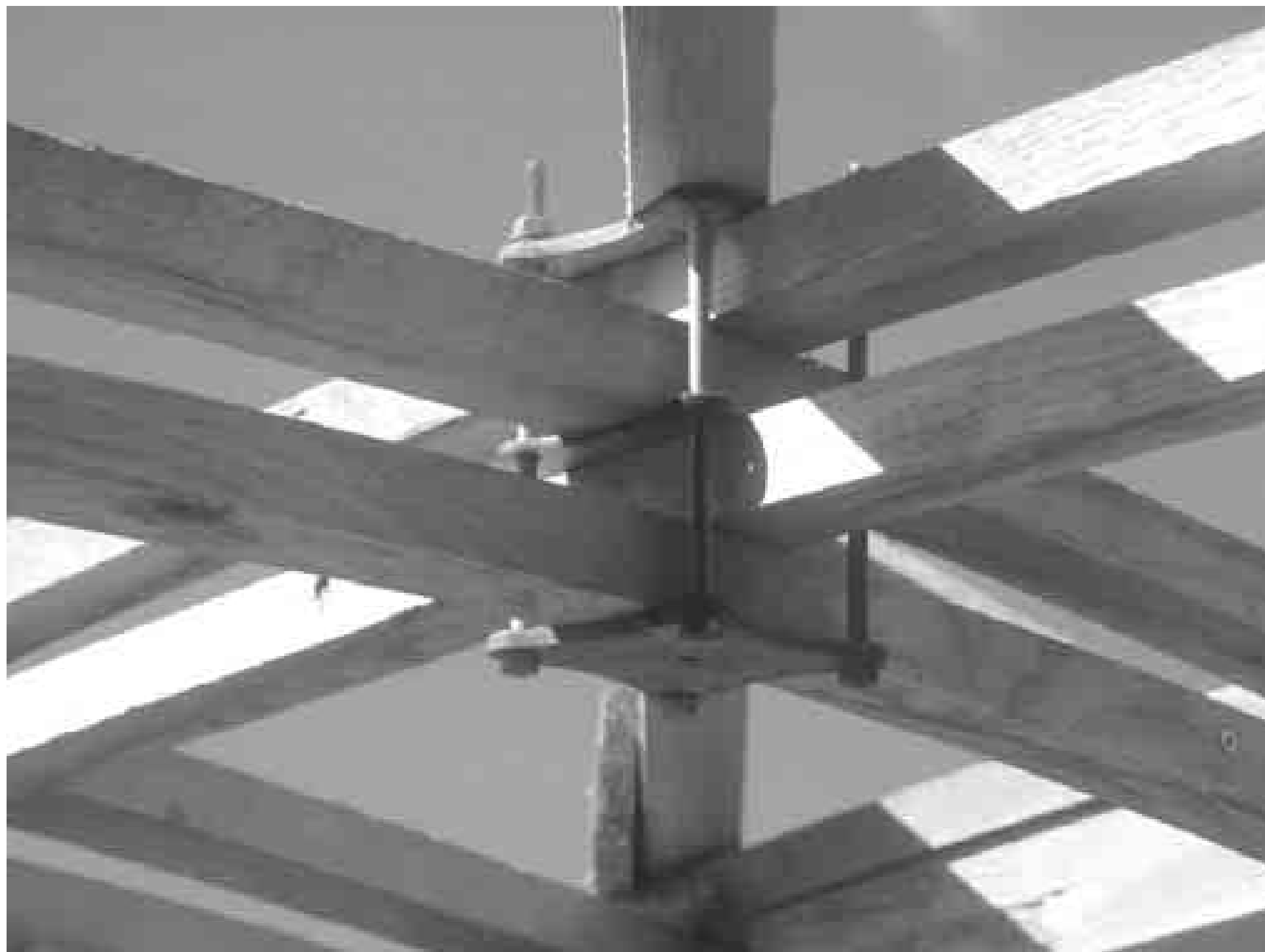
M8 Bolt



Slots in outermost layers
ranging in length from
50mm to 150mm

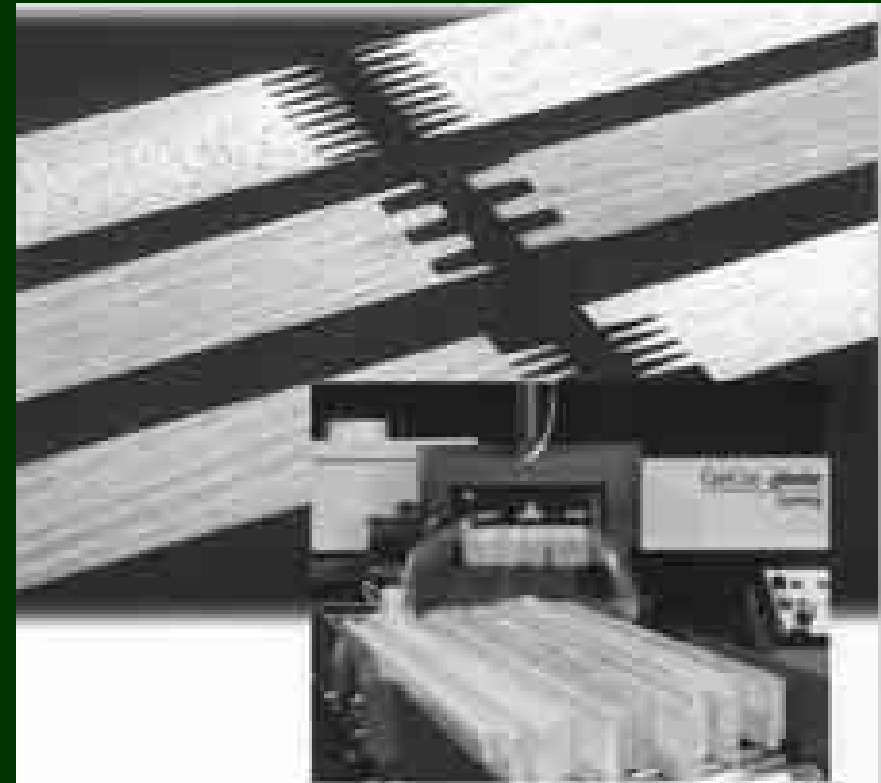








Forming the laths



GreCon *dimter*





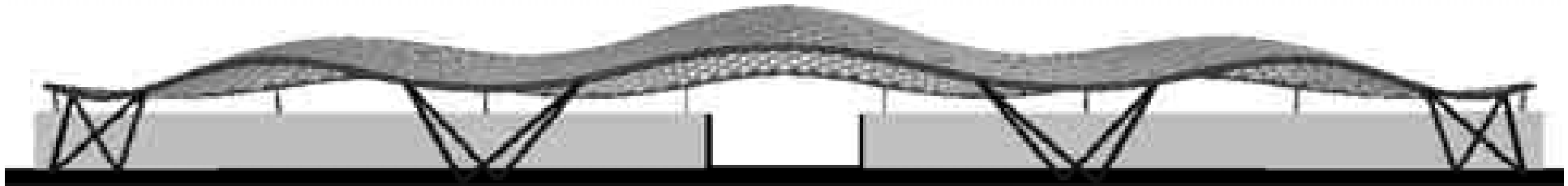








The Savill Building



90m x 25m

4 Layers 80 x 50 mm Larch

Glenn Howells Architects

Engineers HRW

Buro Happold – Roof Engineers



The Savill Building

The challenge:

**To design a large modern building for a
very sensitive site**

To use local timber

The Savill Building

The complication:

**Fixed budget and client / design team
with little experience of innovative design
and construction**

Material with unknown properties

The Savill Building

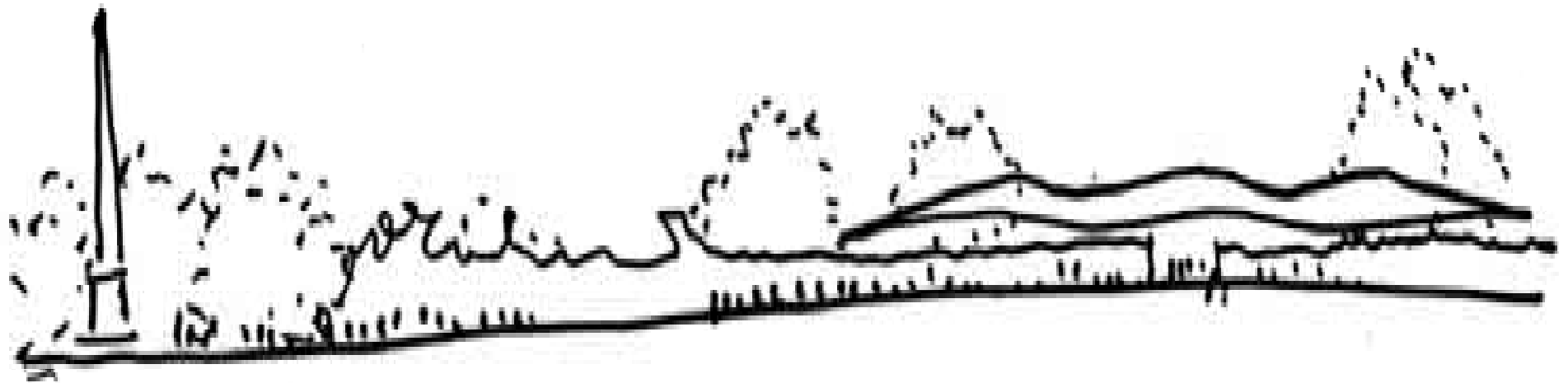
The solution:

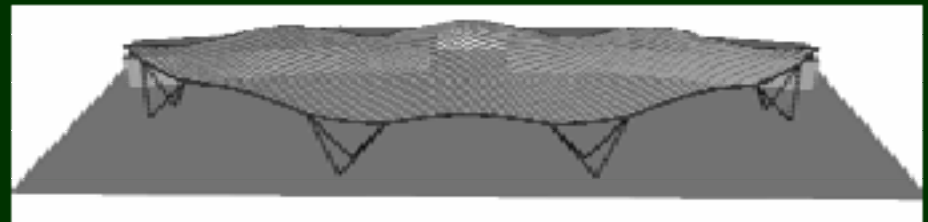
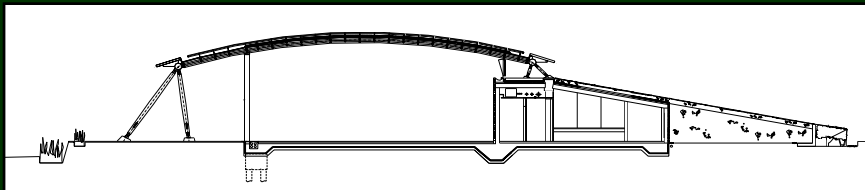
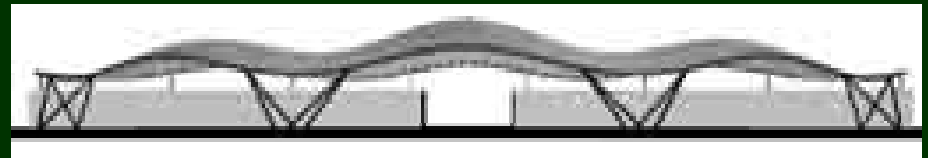
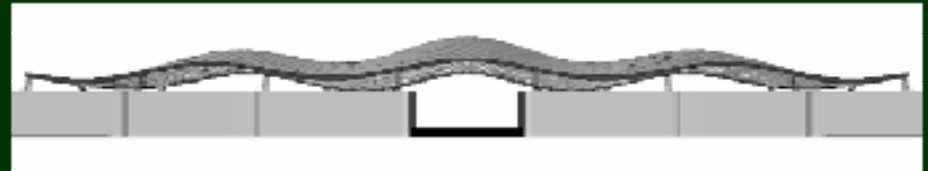
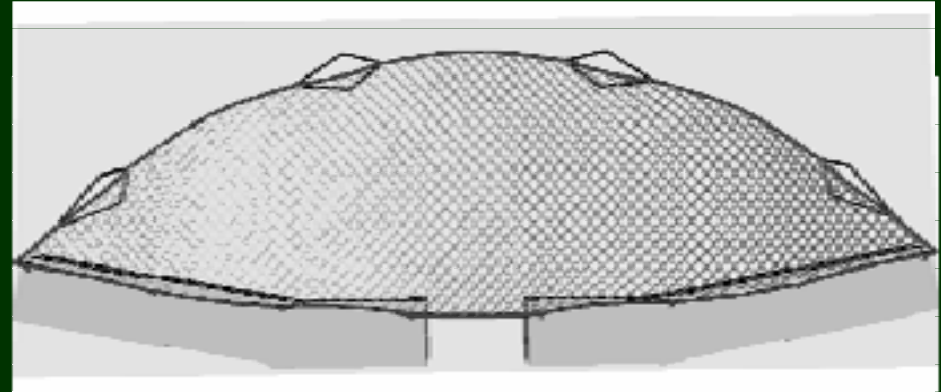
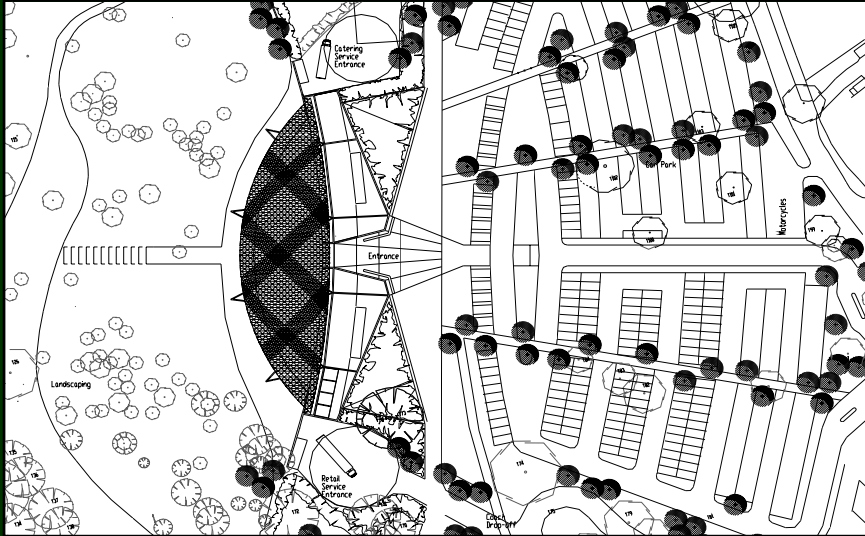
Good communication

Use of EC5 for reliable design outcome

Material testing

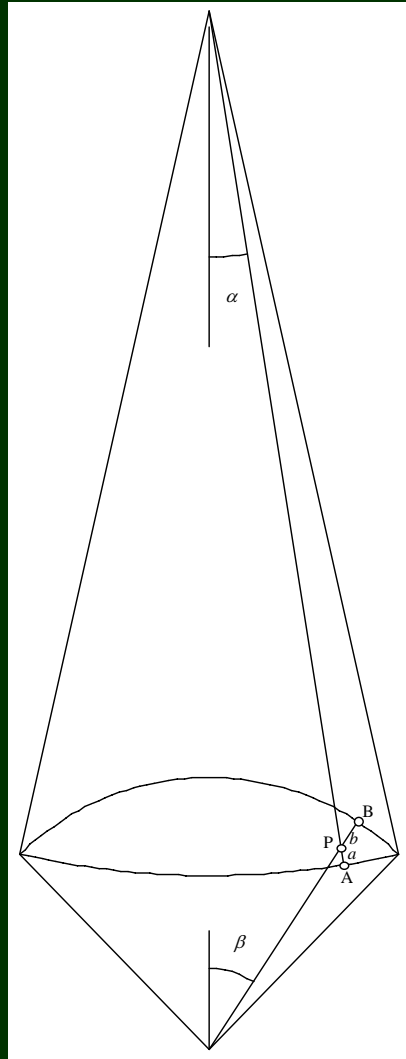
Competition sketch





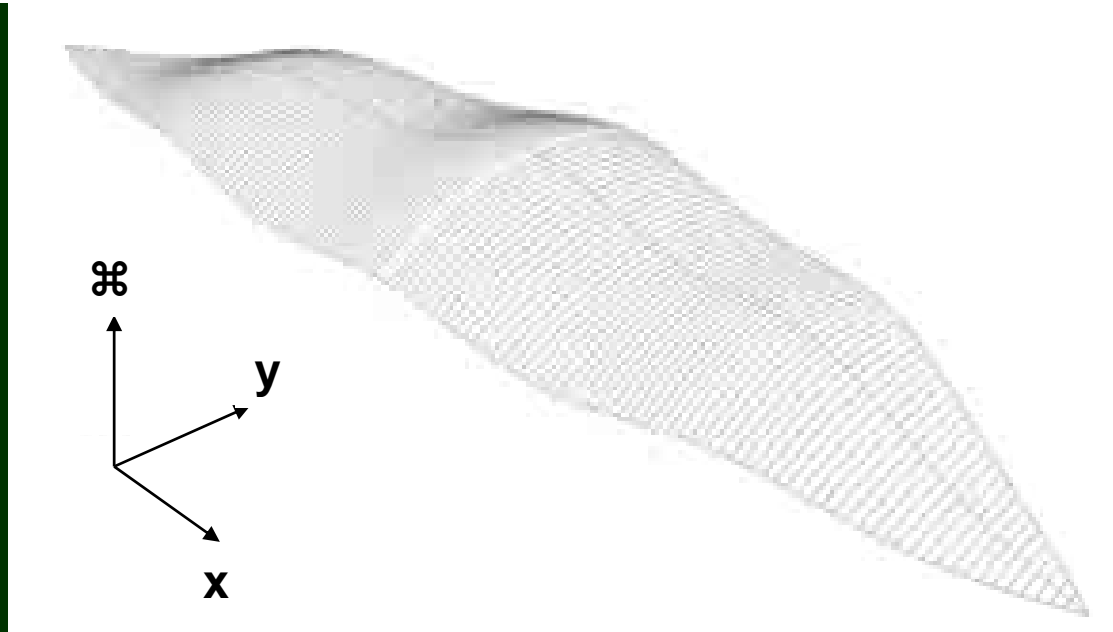
Glenn Howells Architects

Defining the Form – Mathematical



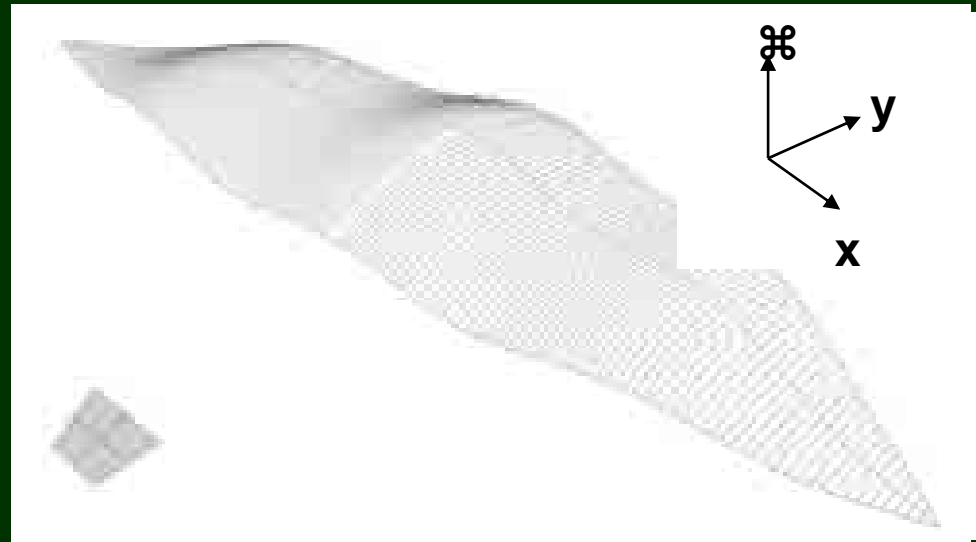
Form-finding with University of Bath

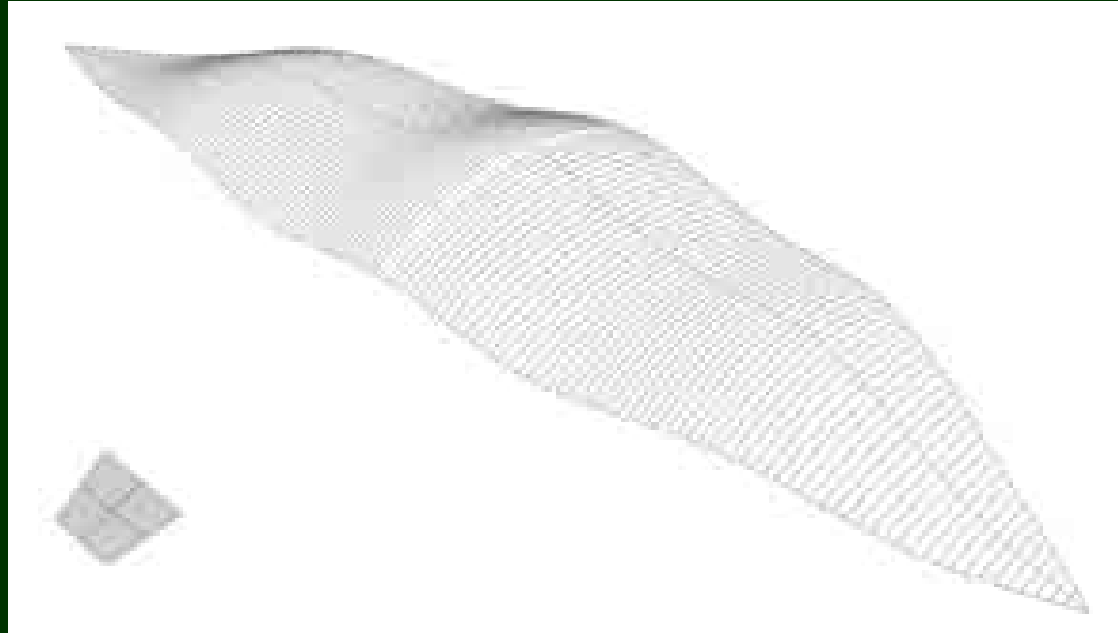
Perimeter slab is set out using arcs of two intersecting circles



- **Curved centreline on plan, midline between the circles.**
- **Centre line of the roof, in section, generated by cosine curve, of varying amplitude (peaks and troughs at the tops of domes and bottoms of valleys).**
- **Cross-section is set out, across the sinusoidal centre line, as series of parabolic curves of varying shape.**

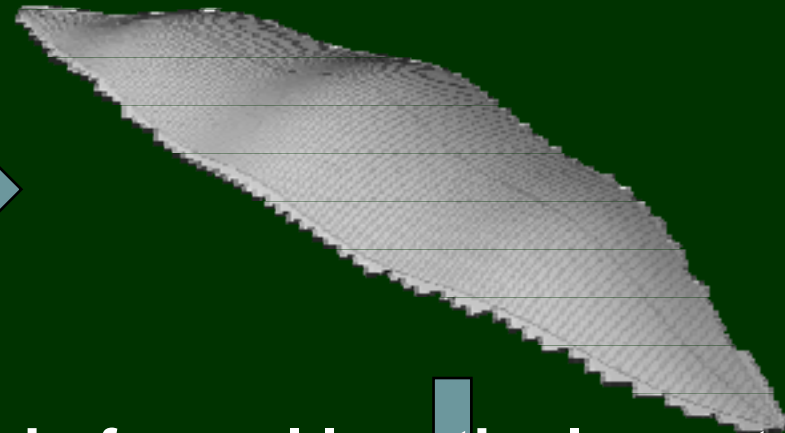
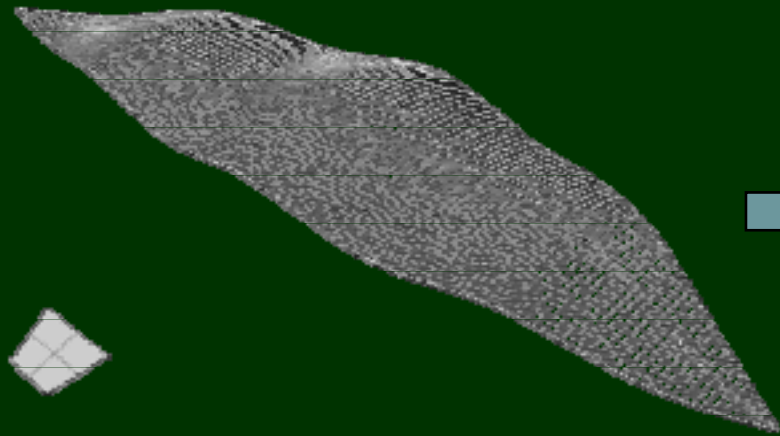
- $z = f(x, y)$ with a damped cosine wave in the x direction and upside down parabolas in the y direction
- clear geometric basis to the surface shape
- architects and engineers could work together to adjust and agree shape to meet aesthetic practical constraints



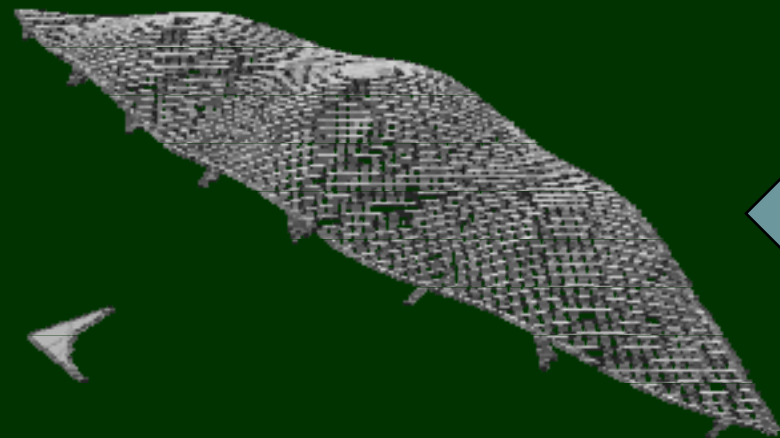


- **Perimeter of shell set out by cutting the surface with planes – thus structural element trimming the edge is bent in only two dimensions**

Defining the Form

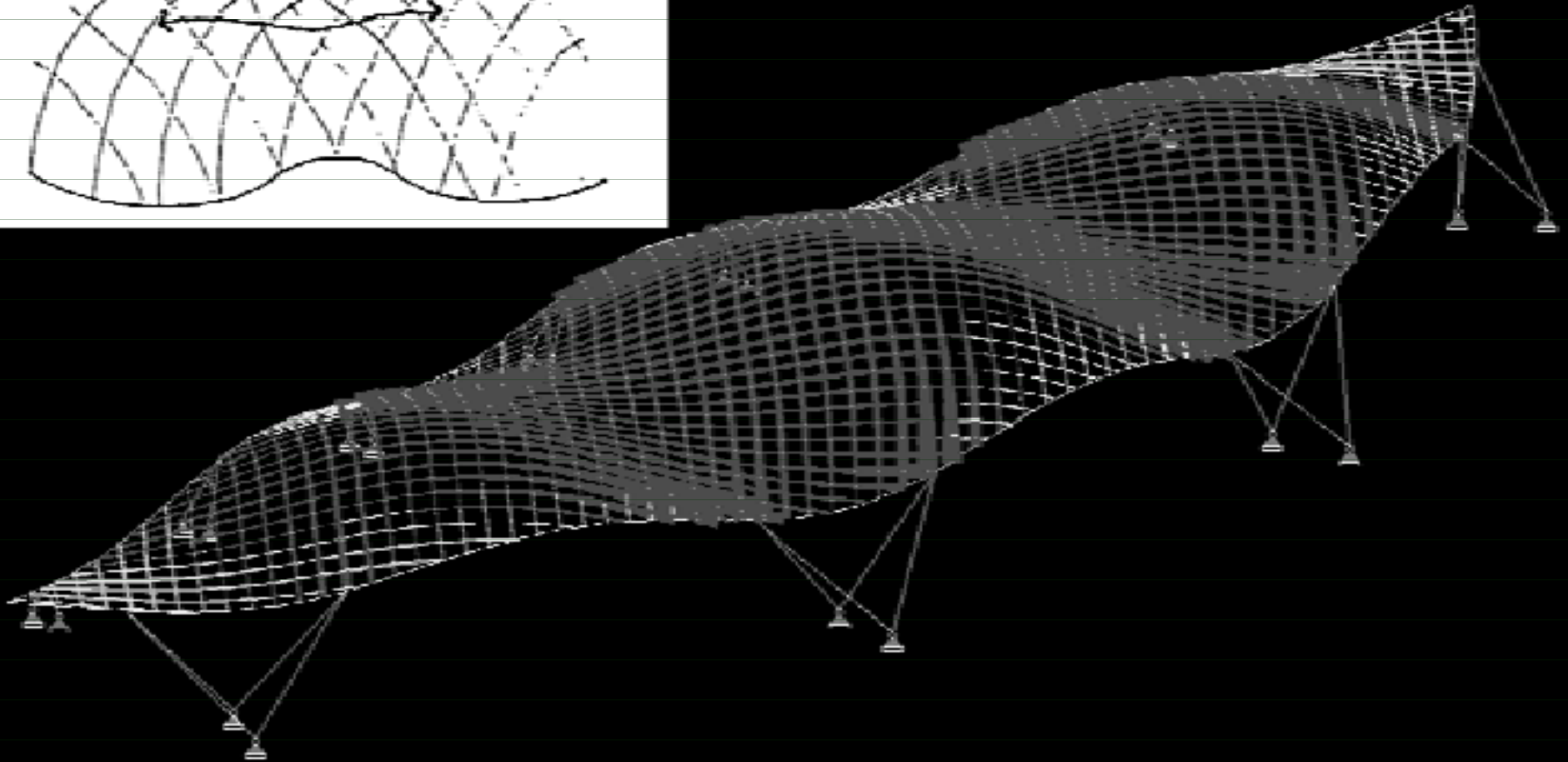


grid of equal length elements by
constructing a Tchebyshev net

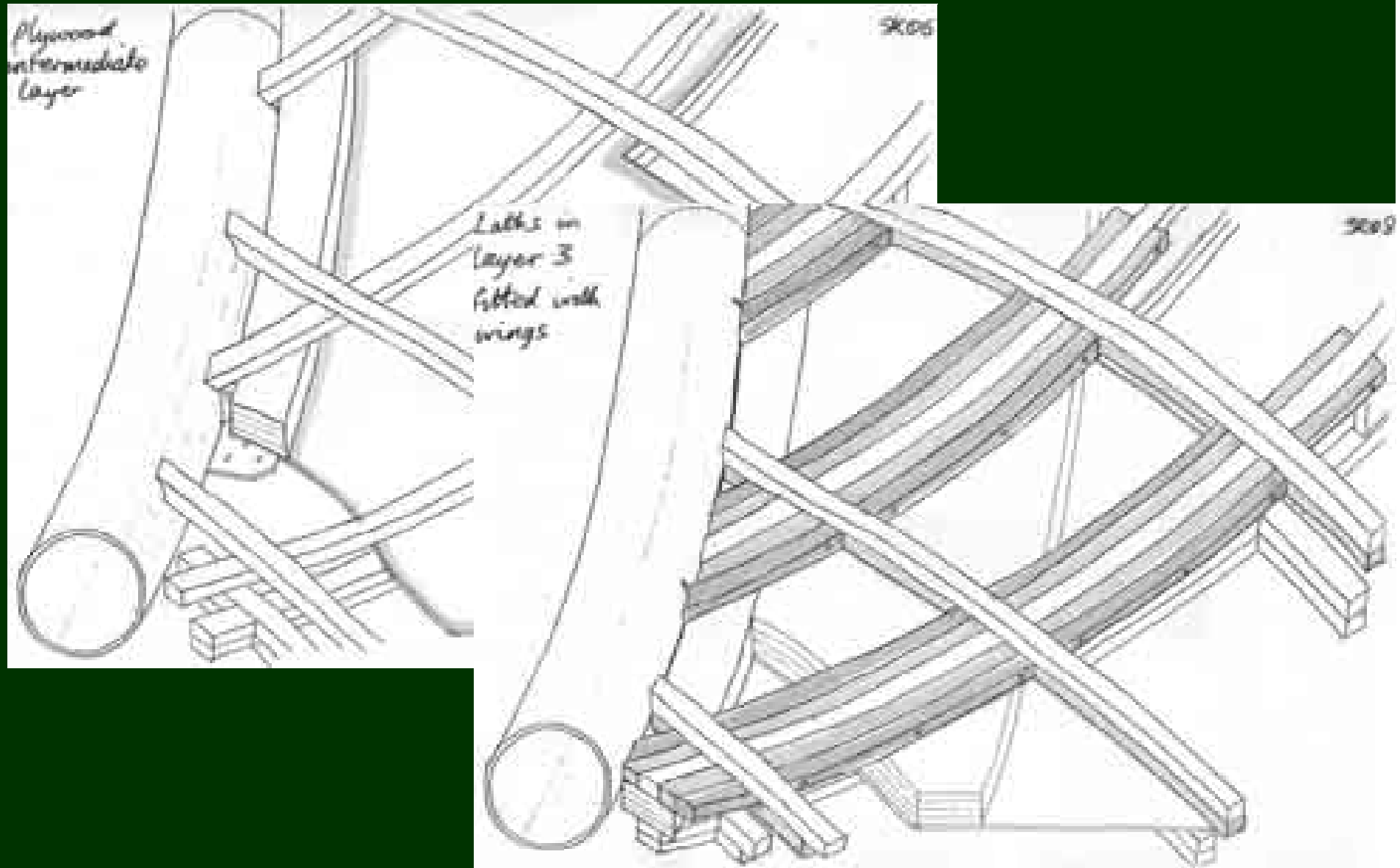


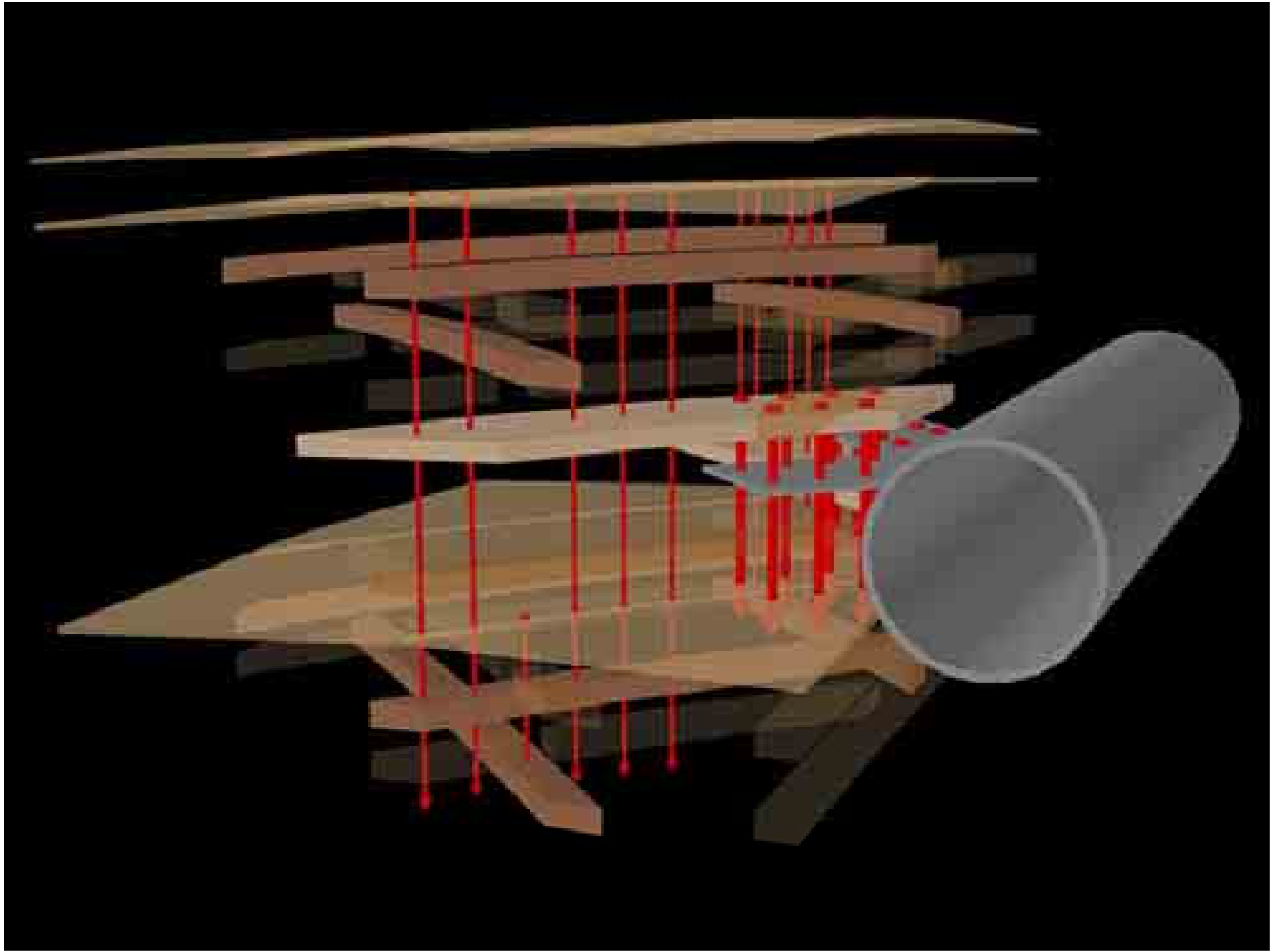
Establishing the Structure

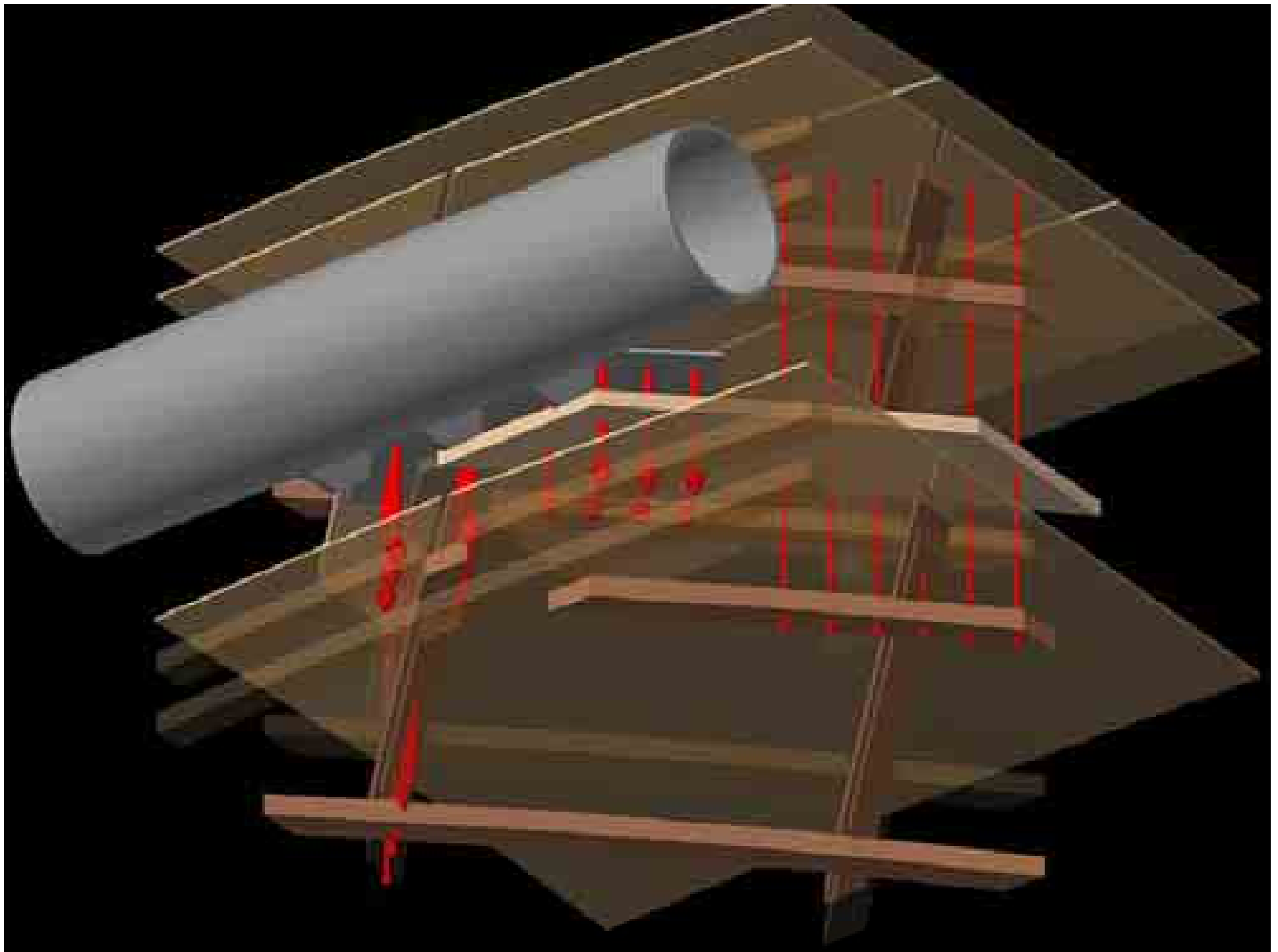
Analysis, Design and Detailing



Edge Detail: Carpentry advice









Timber Testing

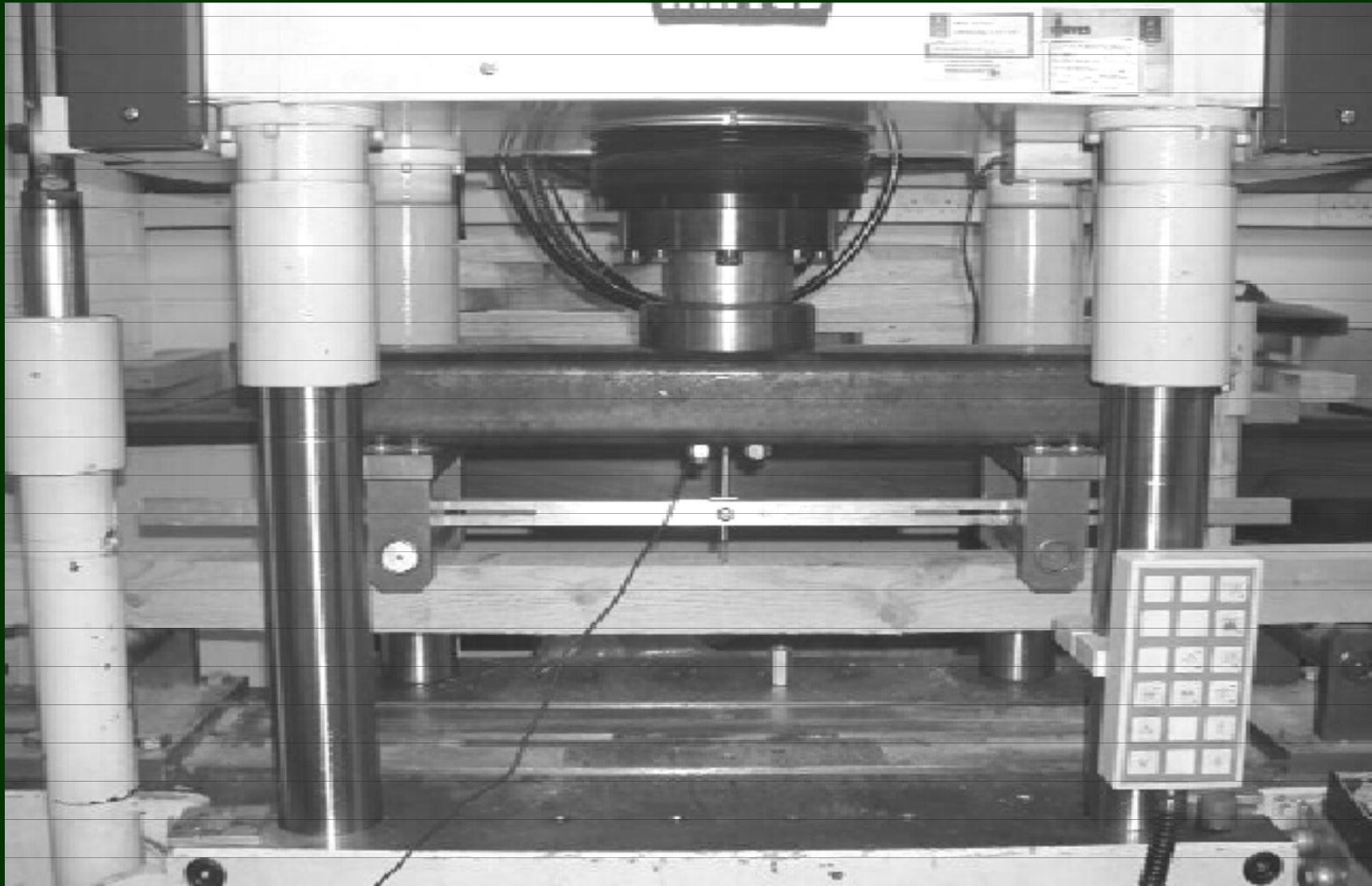
BS EN 384: 1995: Structural timber - Determination of characteristic values of mechanical properties and density

BS EN 408: 1995: Timber structures - Structural timber and glued laminated timber - Determination of some physical and mechanical

Testing by

University of Bath

Timber testing and properties



Determination of properties

Table 1 – Strength classes – Characteristic values																			
		Softwood species												Hardwood species					
		C14	C16	C18	C20	C22	C24	C27	C30	C35	C40	C45	C50	C55	C60	C65	C70	C80	C90
Strength properties (in N/mm ²)																			
Bending	$f_{t,k}$	14	16	18	20	22	24	27	30	35	40	45	50	55	60	65	70	80	90
Tension parallel	$f_{t,k}$	8	10	11	12	13	14	16	18	21	24	27	30	35	40	45	50	55	60
Tension perpendicular	$f_{t,k}$	2.4	2.6	2.8	3.0	3.2	3.4	3.6	3.8	4.2	4.5	4.8	5.2	5.5	6.0	6.5	7.0	7.5	8.0
Compression parallel	$f_{c,k}$	19	21	23	25	27	29	32	35	40	45	50	55	60	65	70	75	80	90
Compression perpendicular	$f_{c,k}$	2.0	2.2	2.3	2.5	2.6	2.8	2.9	3.2	3.5	3.8	4.1	4.2	4.6	4.8	5.0	5.2	5.5	6.0
Shear	$f_{v,k}$	1.7	1.9	2.0	2.2	2.4	2.5	2.8	3.0	3.4	3.8	3.9	4.3	4.6	4.8	5.0	5.2	5.5	6.0
Stiffness properties (in N/mm ²)																			
Mean modulus of elasticity parallel	$E_{0,mean}$	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	26
5% modulus of elasticity parallel	$E_{0,5}$	4.7	5.4	6.2	6.8	7.7	8.4	9.3	10	11	12	13	14	15	16	17	18	19	22
Mean modulus of elasticity perpendicular	$E_{0,mean}$	0.22	0.27	0.30	0.32	0.35	0.37	0.39	0.40	0.43	0.47	0.50	0.52	0.54	0.56	0.58	0.60	0.62	0.70
5% modulus of elasticity perpendicular	$E_{0,5}$	0.14	0.17	0.19	0.20	0.22	0.23	0.24	0.25	0.26	0.28	0.30	0.31	0.32	0.33	0.34	0.35	0.36	0.40
Mean shear modulus	$G_{0,mean}$	0.44	0.5	0.56	0.59	0.65	0.69	0.72	0.75	0.81	0.88	0.94	1.00	1.05	1.10	1.15	1.20	1.25	1.40

Density (in kg/m ³)																			
Density	ρ_k	290	310	330	350	370	390	410	430	450	470	490	510	530	550	570	590	610	630
Mean density	ρ_{mean}	350	370	390	410	430	450	470	490	510	530	550	570	590	610	630	650	670	690
Notes		<p>a) Values given apply to tension strength, compression strength, shear strength, 5% modulus of elasticity, mean modulus of elasticity, perpendicular to grain and mean shear modulus. Values have been calculated using the following grain to stress ratio</p> <p>b) The characteristic modulus, $E_{0,5}$, is not applicable to timber. It is a statistical constant parameter with a characteristic of 5% and a relative humidity of 65%</p> <p>c) Timber conforming to classes C40 and C50 may not be readily available.</p>																	

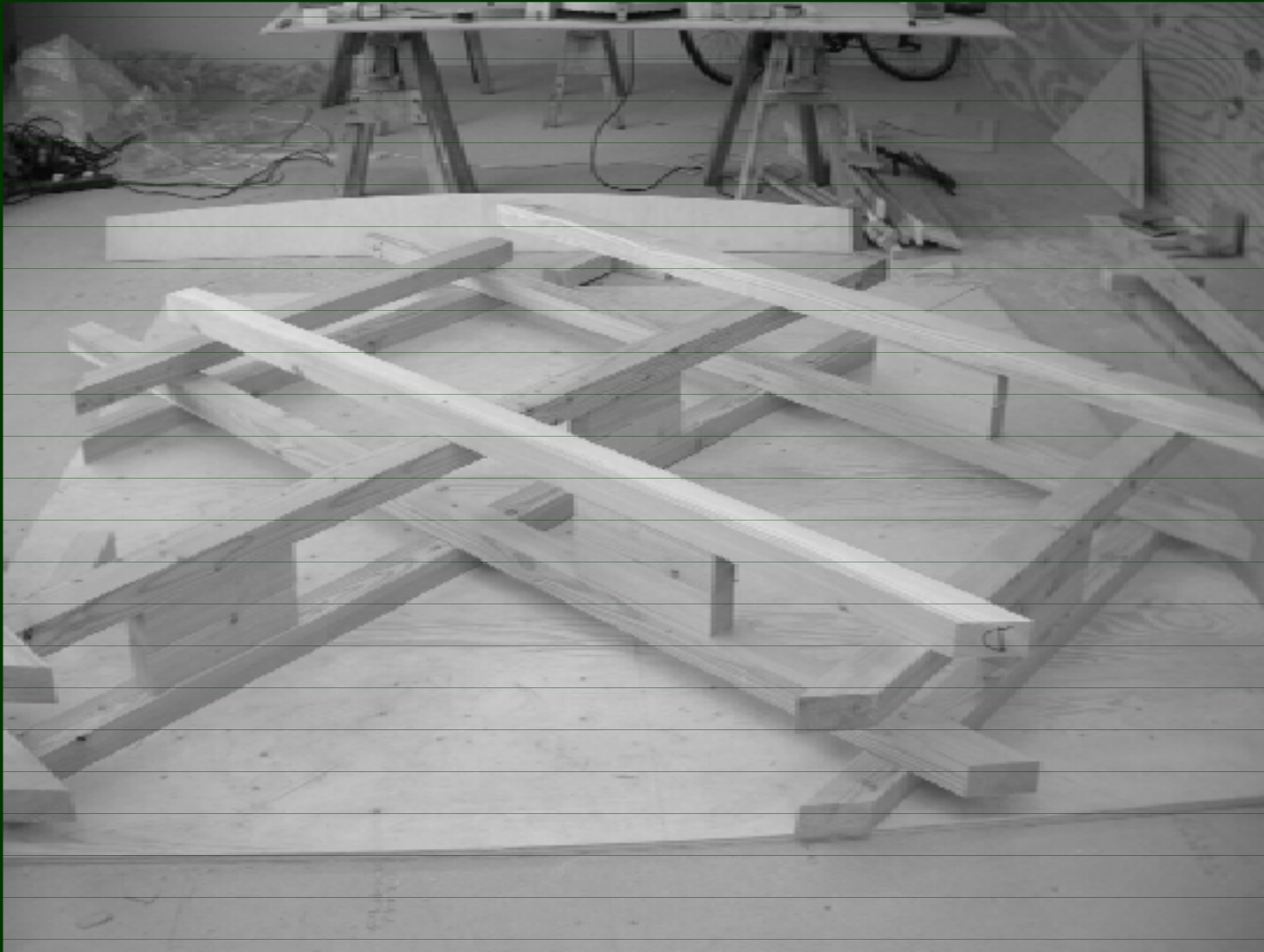
BS EN 338 Structural timber – Strength classes

Savill Building Grade I and Grade II



Sapwood excluded - protective treatment of roof timbers against house longhorn beetle

Design Development - prototyping



Full Size Section of shell



Full Size Section of shell



Roof Construction



Finger jointing

Finished product



Grade and check m.c.

Grade 1 Larch



Grade 2 Larch









Lay out bottom mat of two layers



Lower into position



Bolt edge plates into position



Bring edge of mat onto plates







Fix Shear Blocks



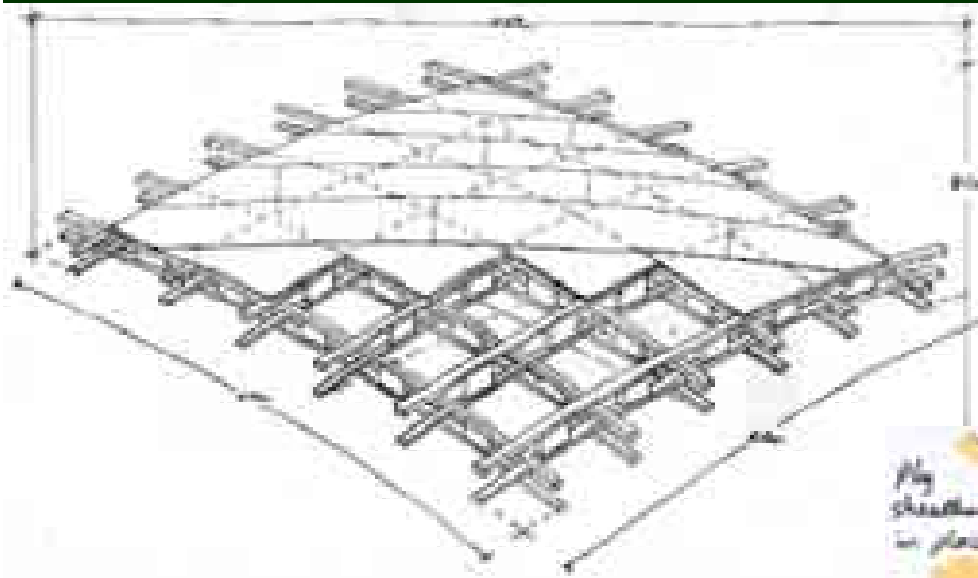
Fix Shear Blocks





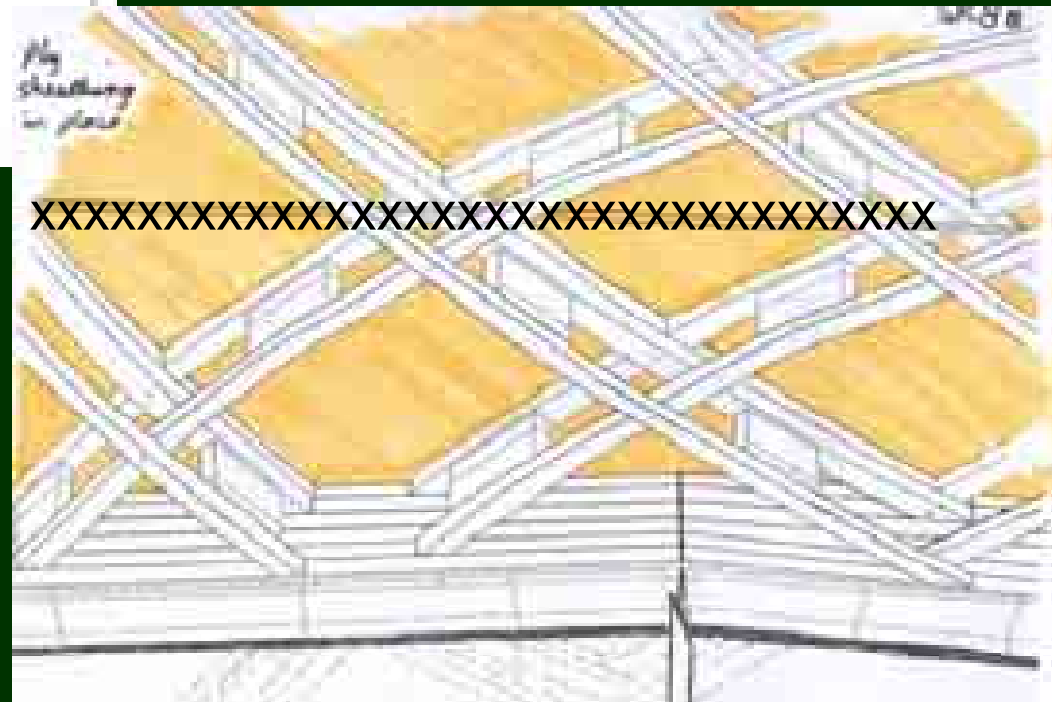


Bracing of shell



**Local larch for structure,
local oak for rain screen**

Bracing: 2 layers 12mm birch ply



Plywood skin – structural bracing



Strike the scaffold



Glazing and Rainscreen

Oak Cladding





Oak cladding



Edge detail



Finished Building





The Garden Context





















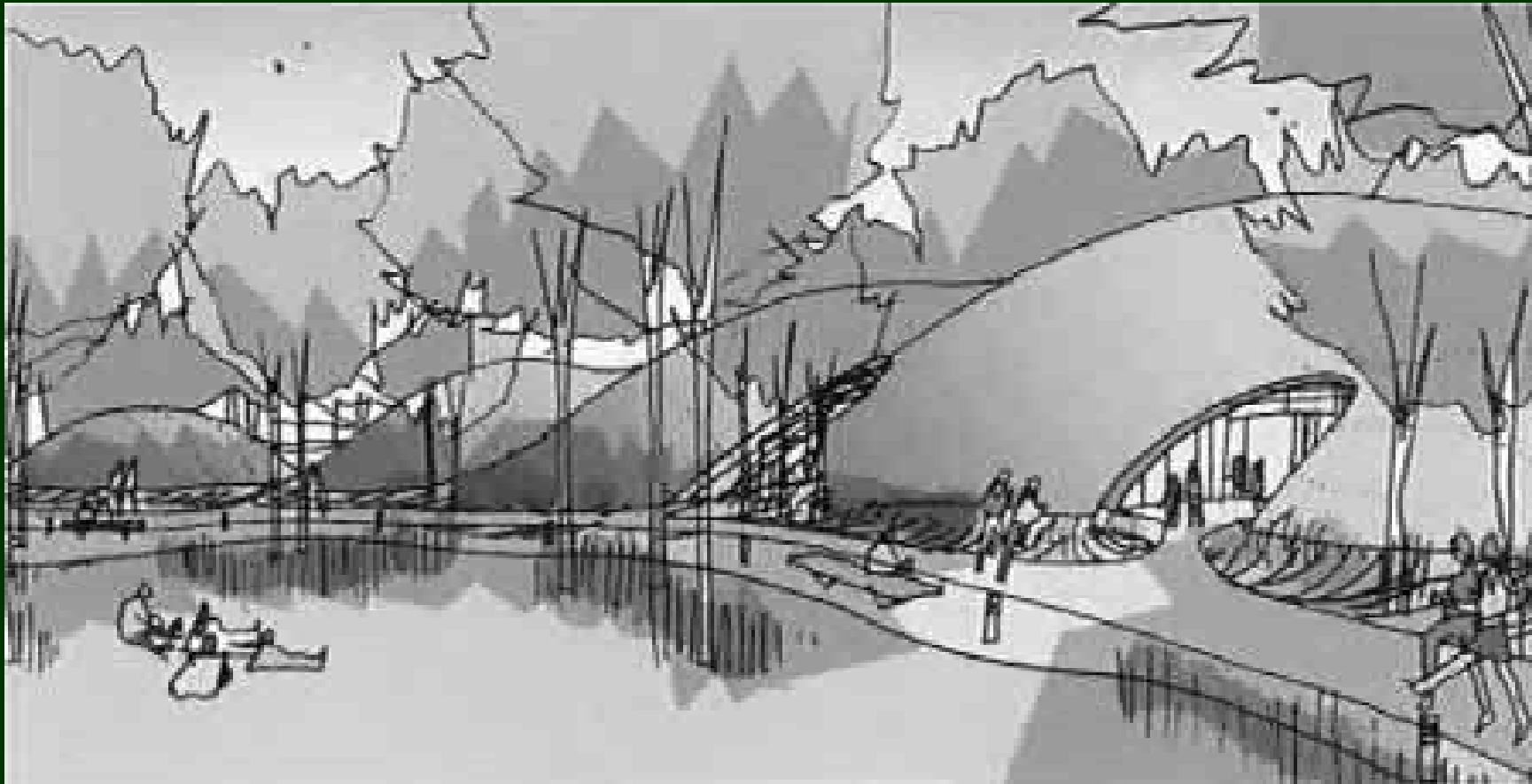


another gridshell

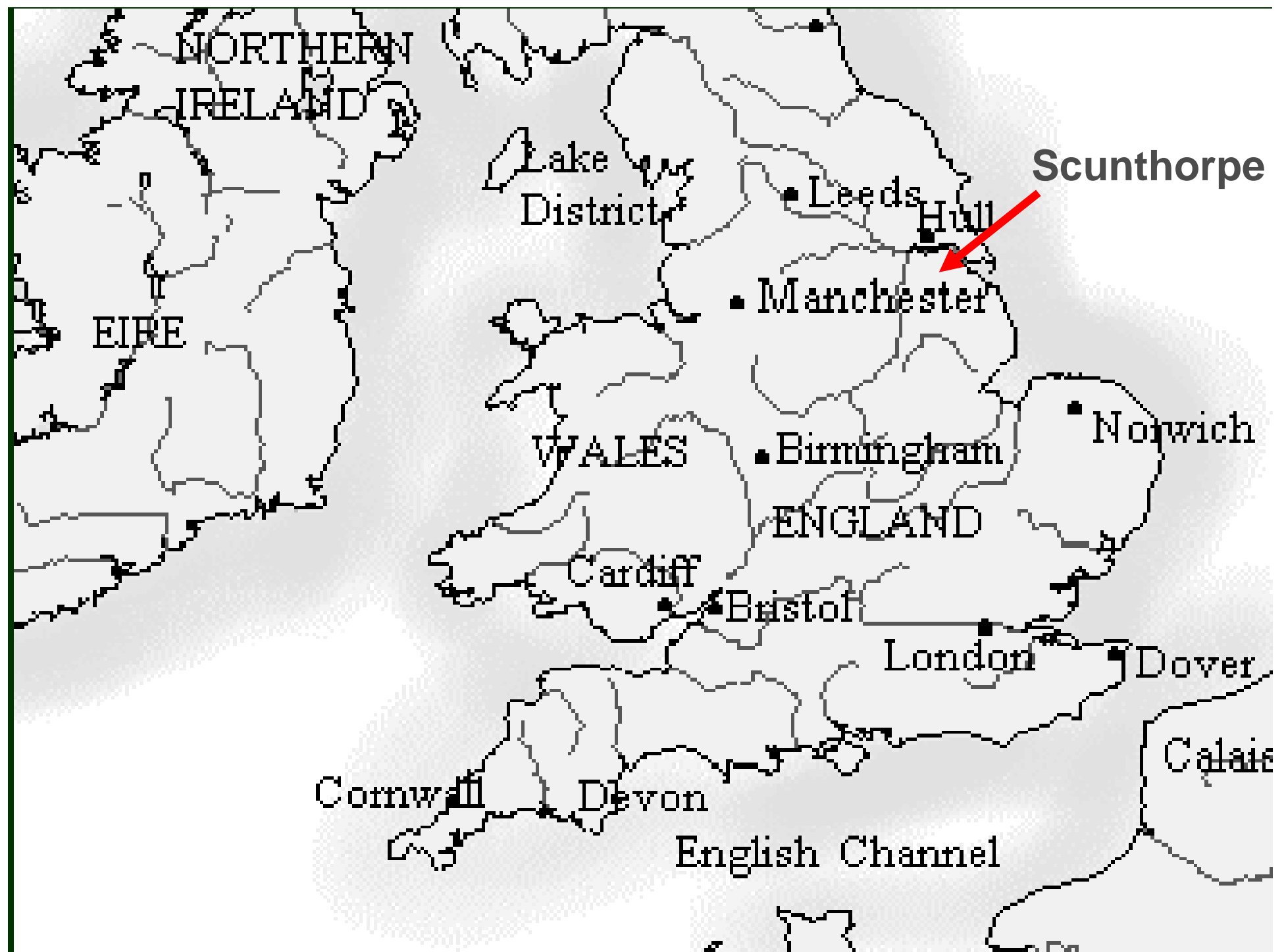
Chiddingstone Castle Orangery



Another Challenge



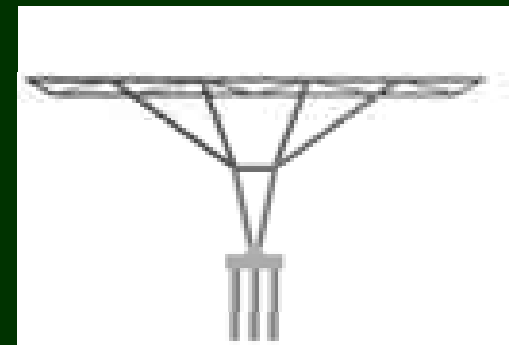
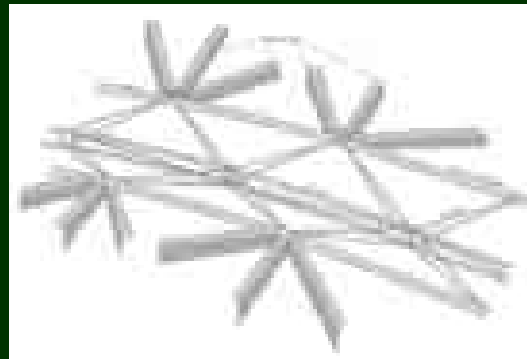
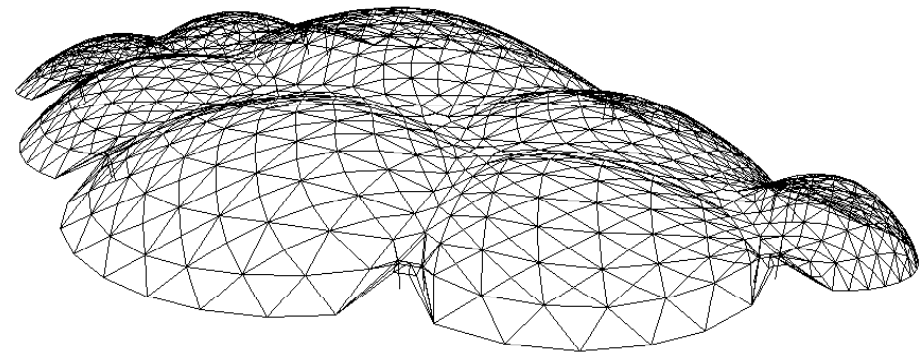
Andrew Wright Associates with S&P Architects Architects



The Scheme



The Competition



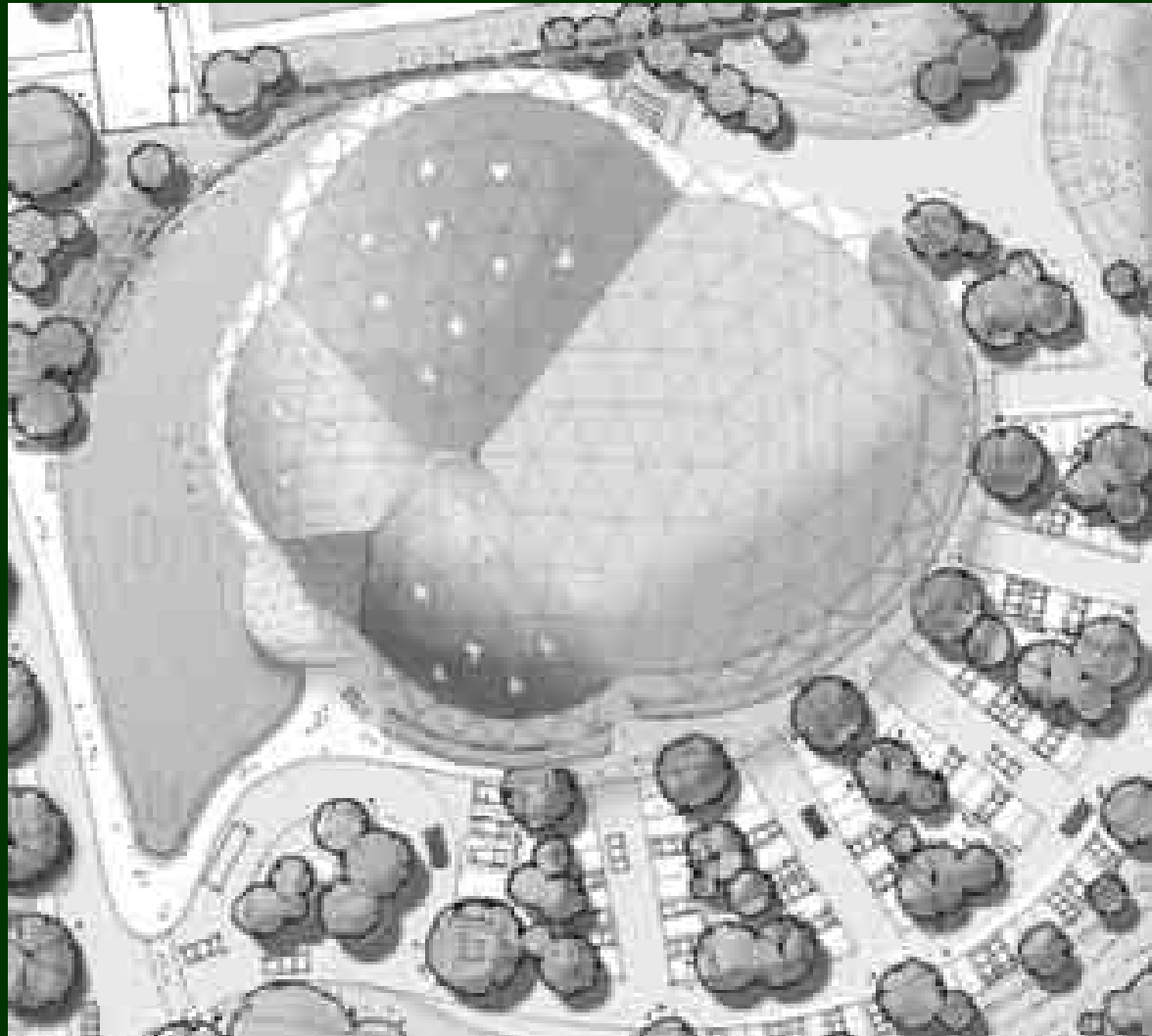
The Scheme



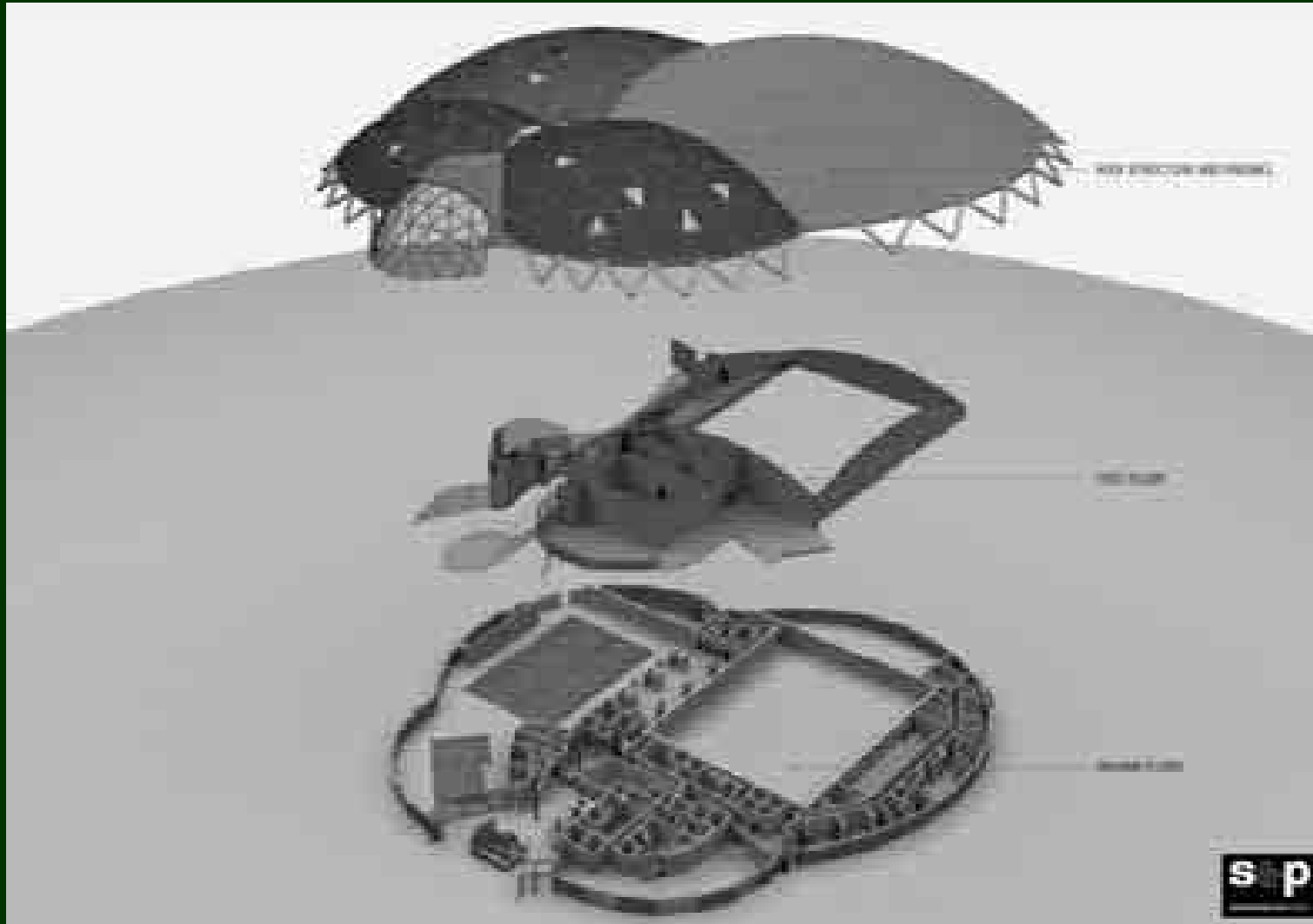
Precedent – Timber Geodesics



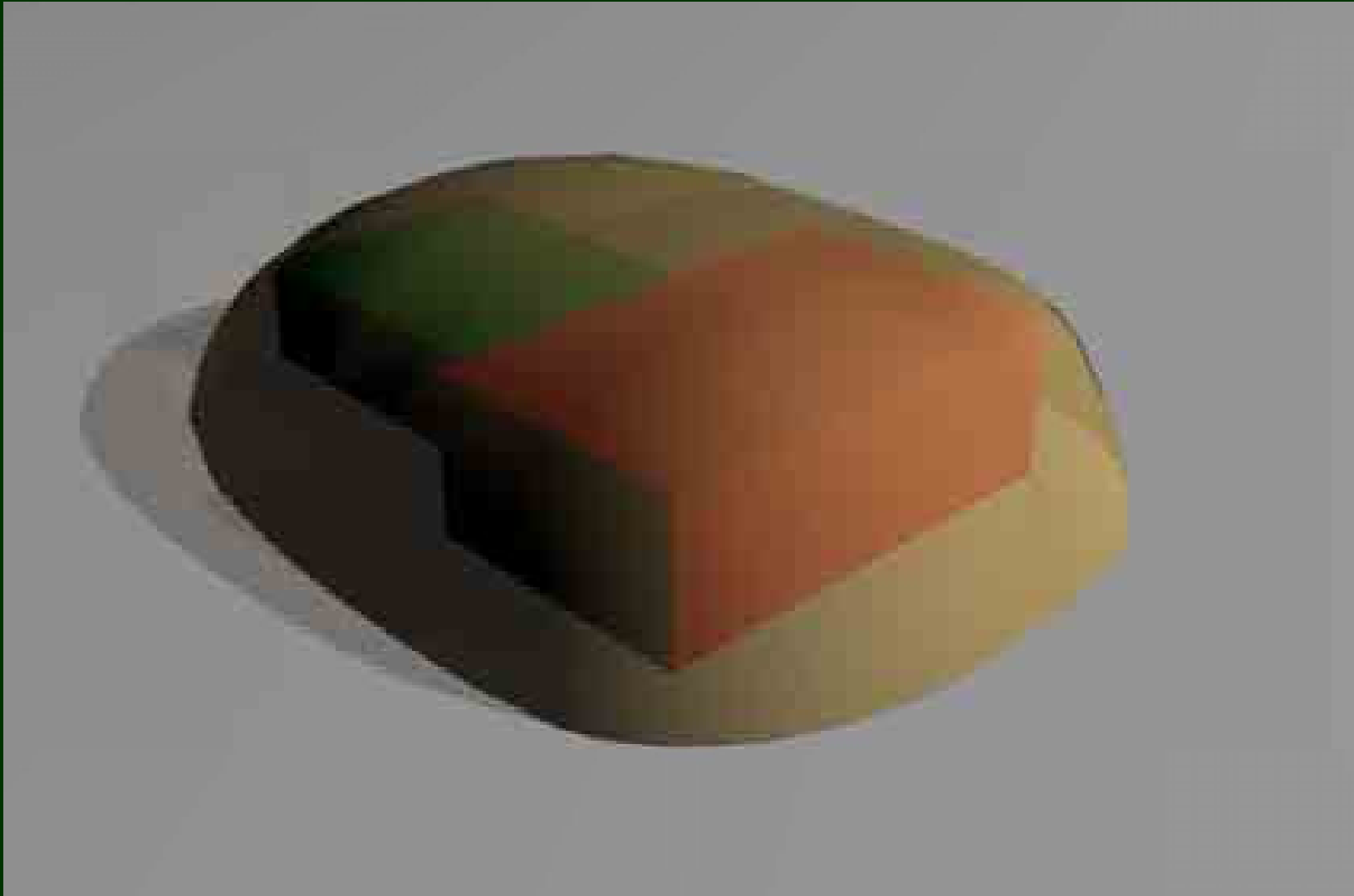
The Scheme



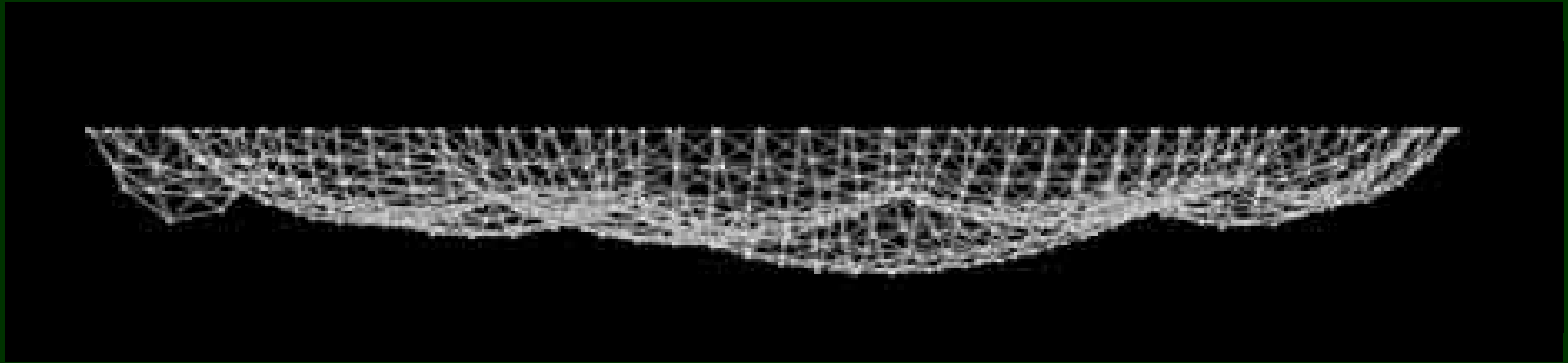
The Scheme – Exploded



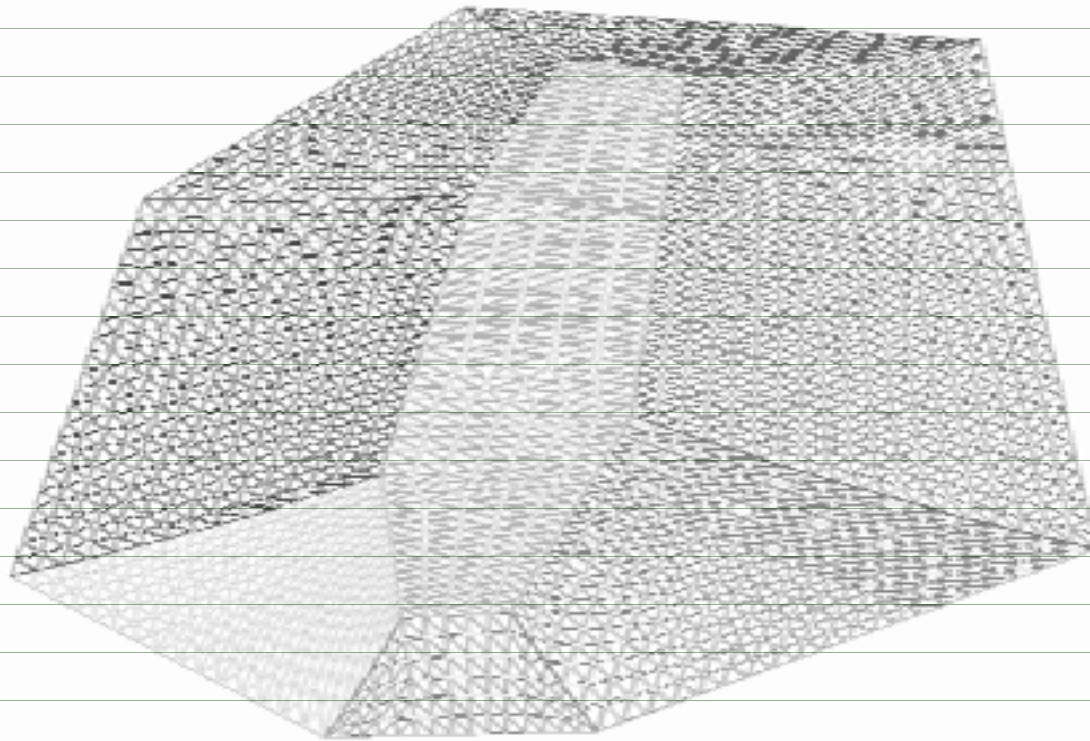
Defining the Roof Surface



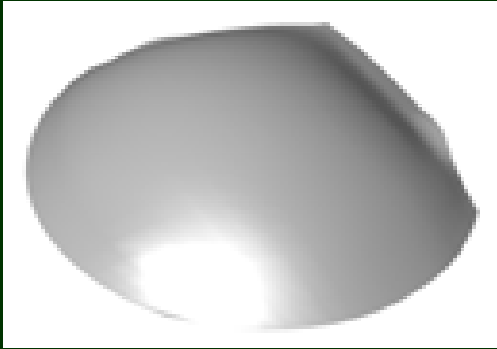
Formfinding – Tenysl ‘Hanging Chain model’



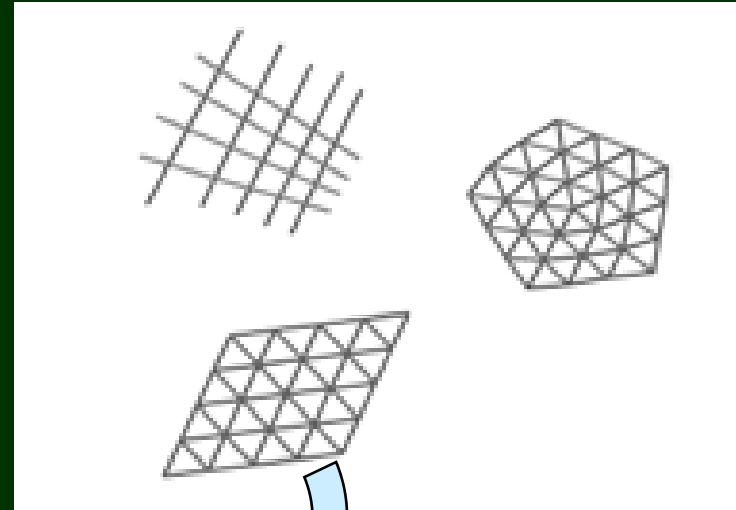
Defining the Roof Surface



Defining the Roof Grid

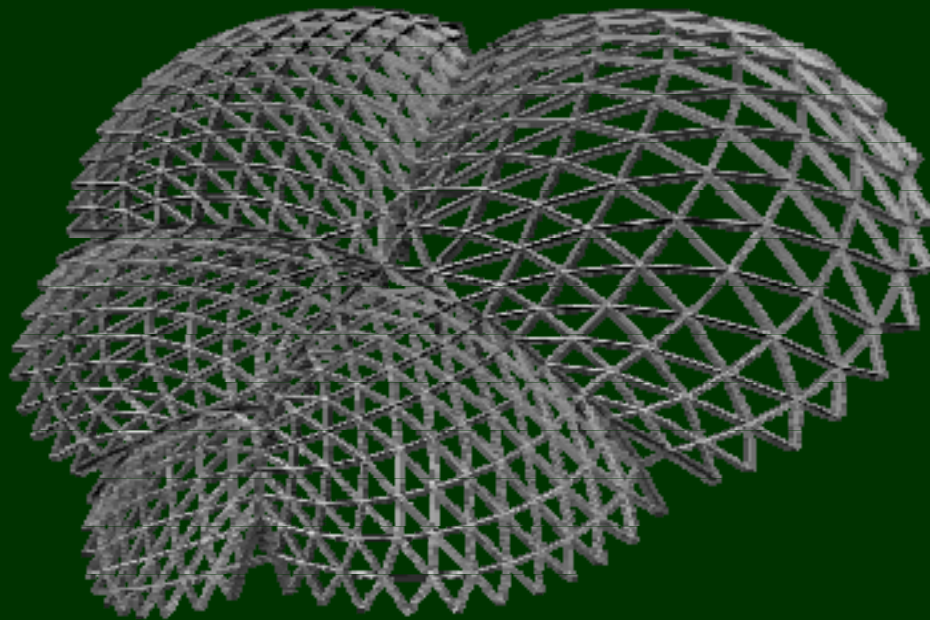


define a
grid

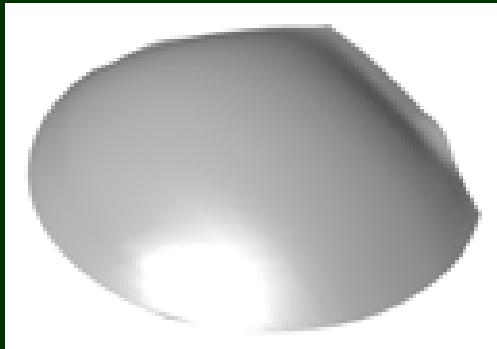


map grid
onto surface

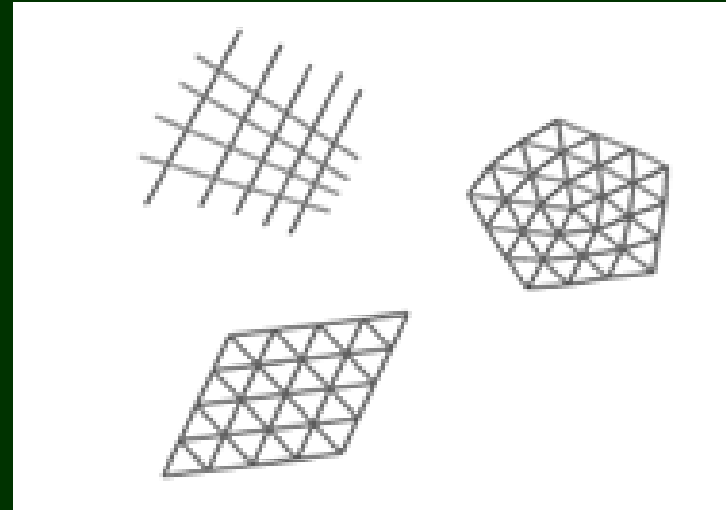
take surface



Defining the Roof Grid

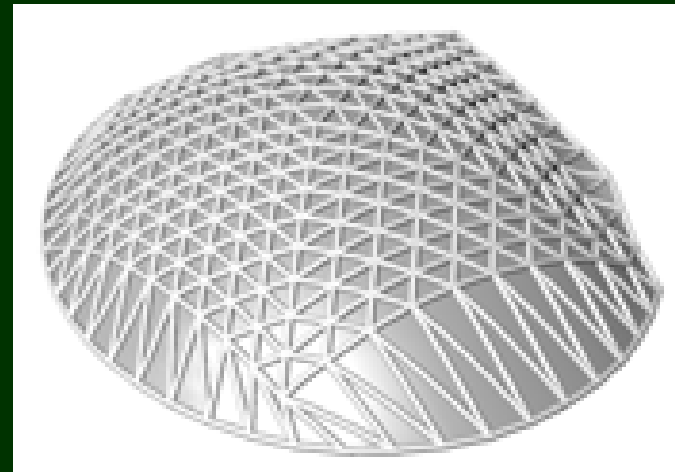
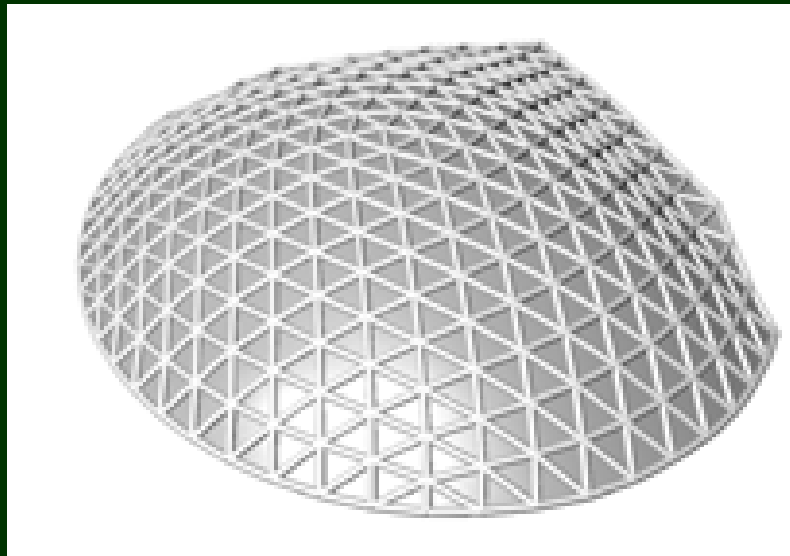


define a
grid



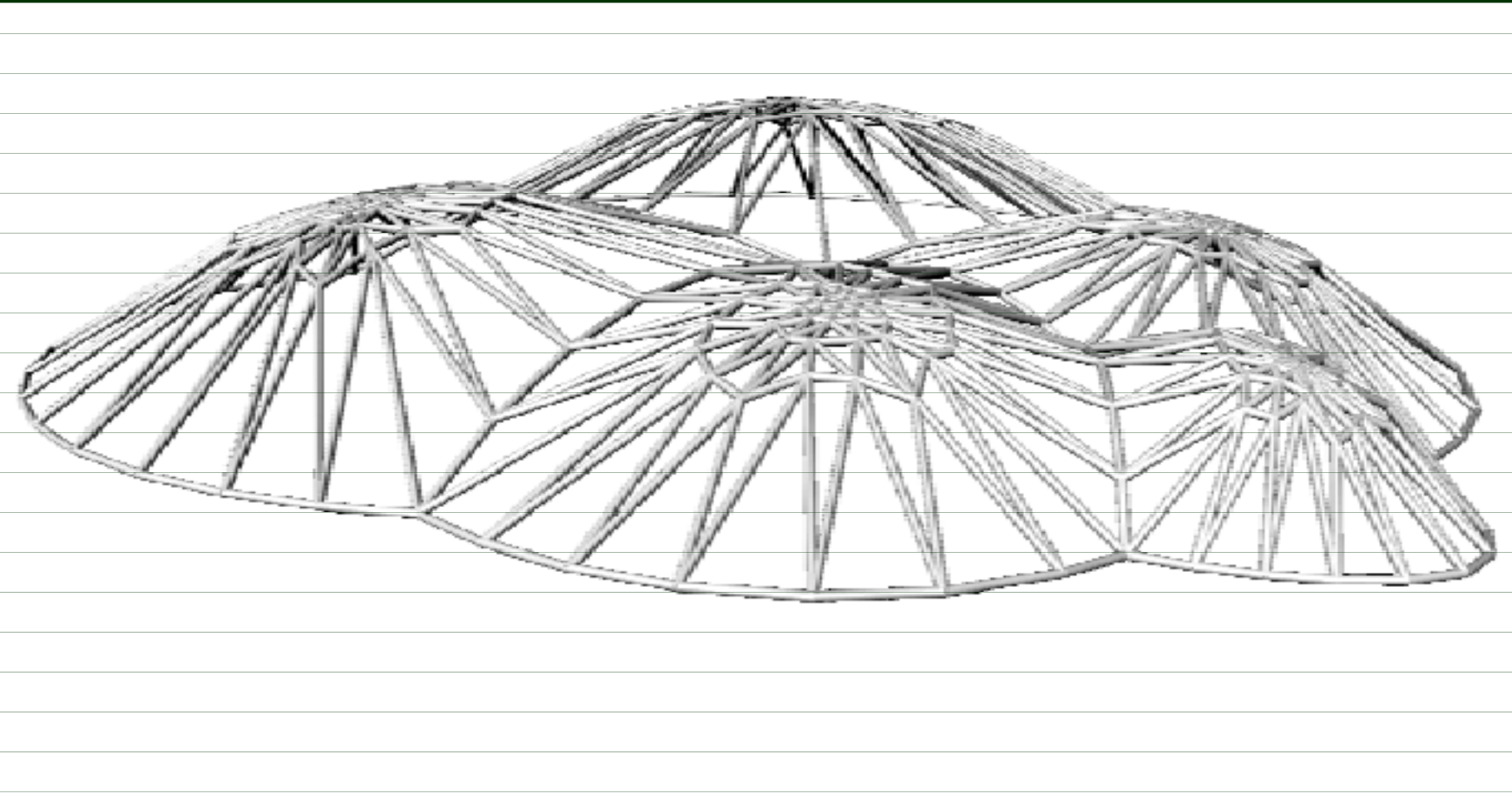
map grid
onto surface

take surface

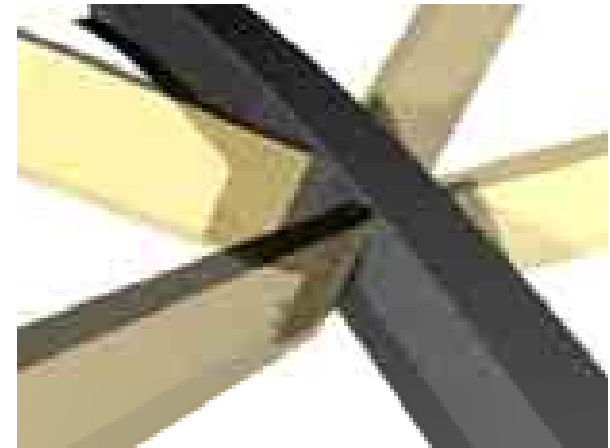
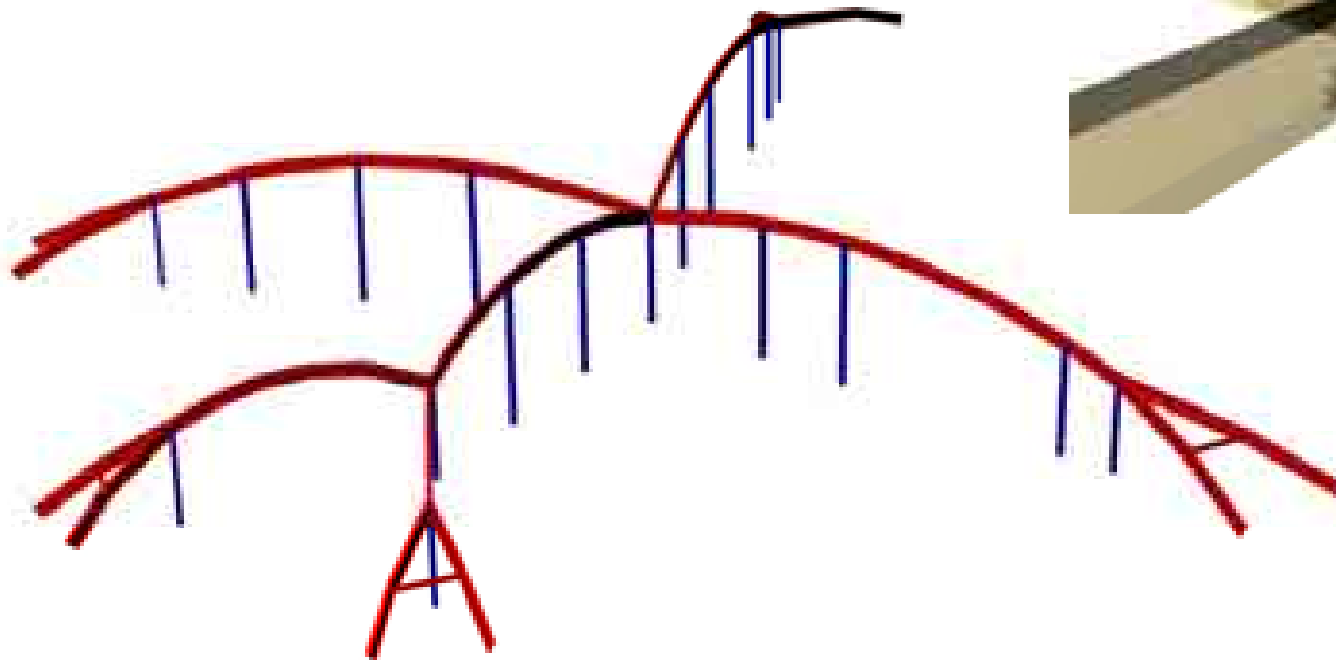


relax grid using dynamic relaxation

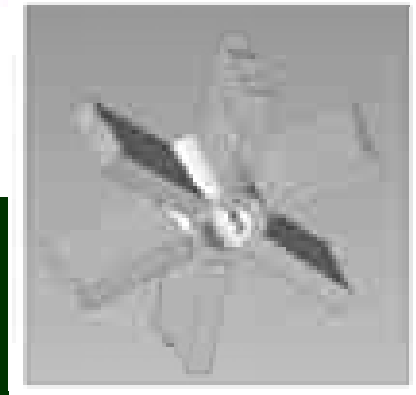
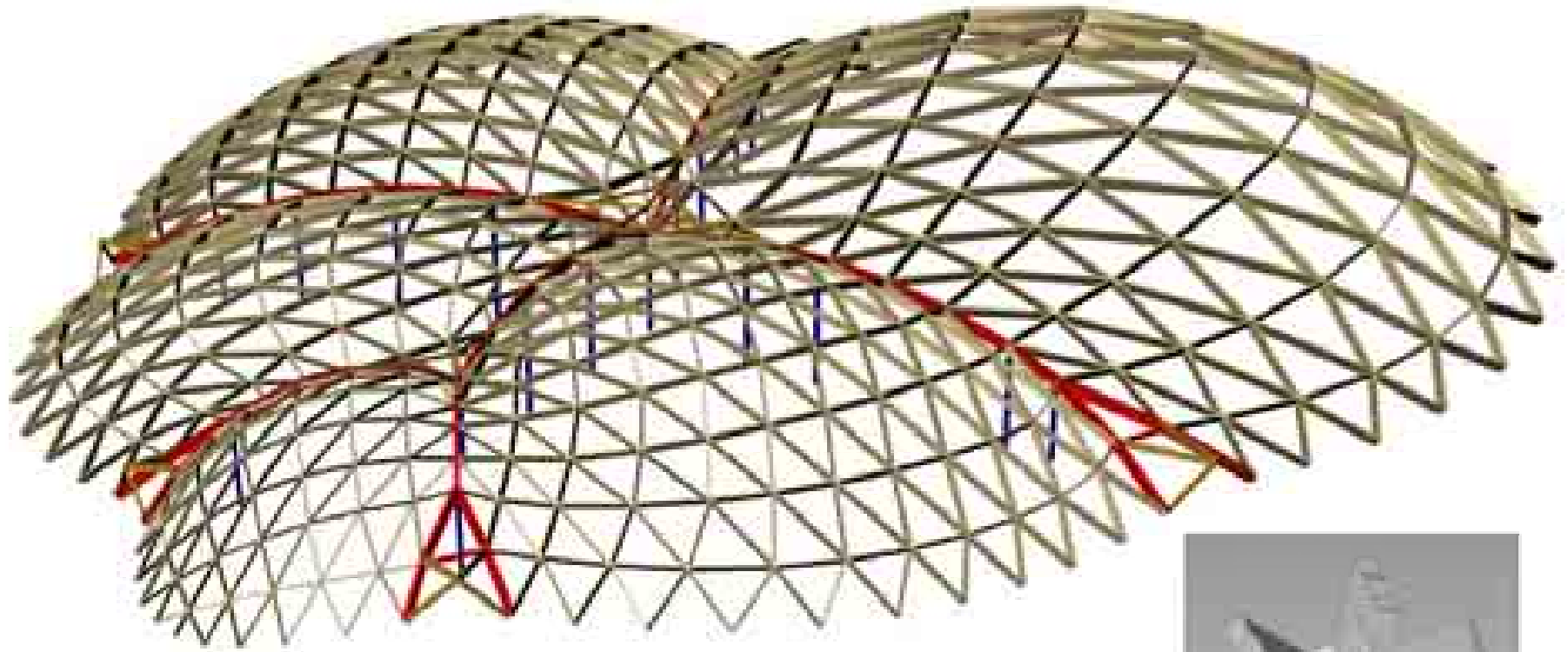
Defining the Roof Grid



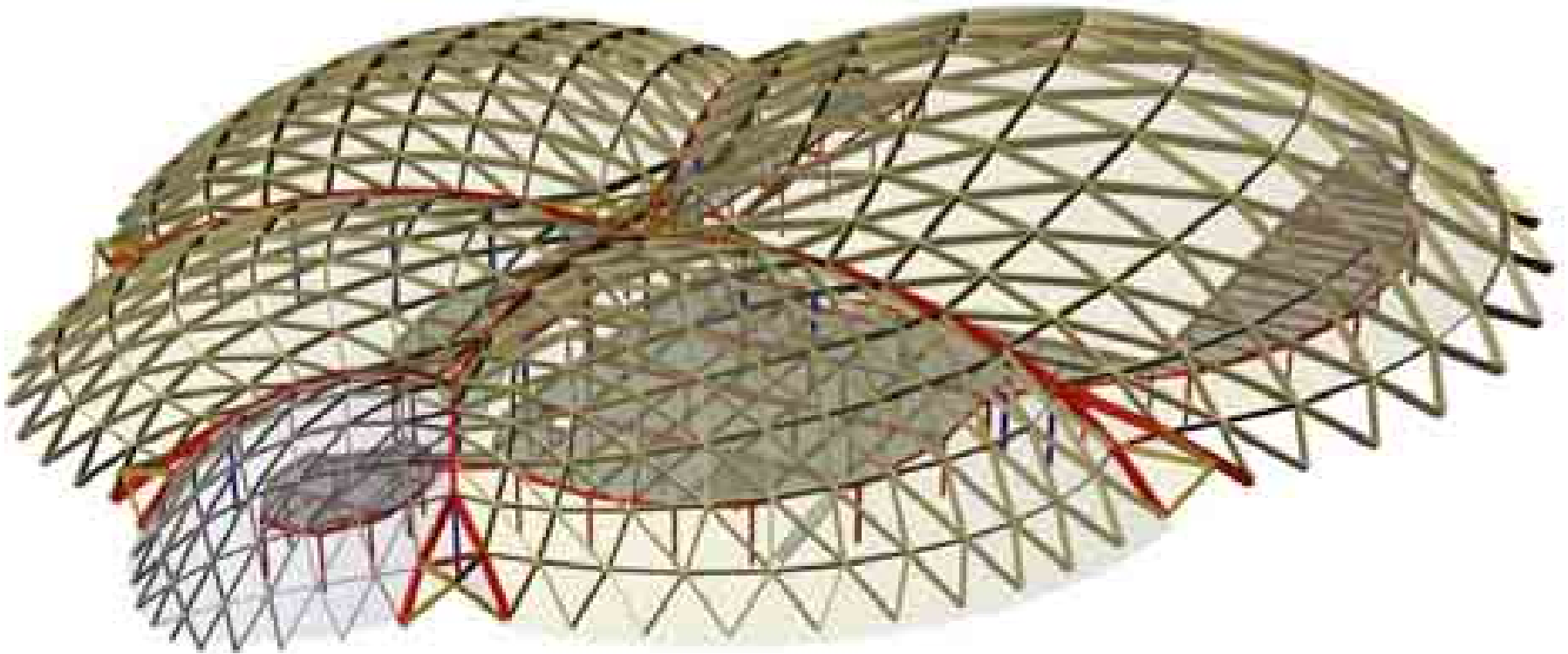
The Structural Solution - Roof



The Structural Solution - Roof



The Structural Solution



The Structural Solution - Cladding

